

# Mechanics of Irregular Honeycomb Structures

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Sixth International Congress on Computational Design Optimization and Simulation, 2016, IIT Bombay, India



Swansea University  
Prifysgol Abertawe



## 1 Introduction

- Regular Honeycomb

## 2 Equivalent elastic properties of random irregular honeycombs

- Longitudinal Young's modulus ( $E_1$ )
- Transverse Young's modulus ( $E_2$ )
- Poisson's ratio  $\nu_{12}$
- Poisson's ratio  $\nu_{21}$
- Shear modulus ( $G_{12}$ )

## 3 Uncertainty modelling and simulation

## 4 Results and discussions

- Numerical results for the homogenised in-plane properties
- Main observations

## 5 Conclusions





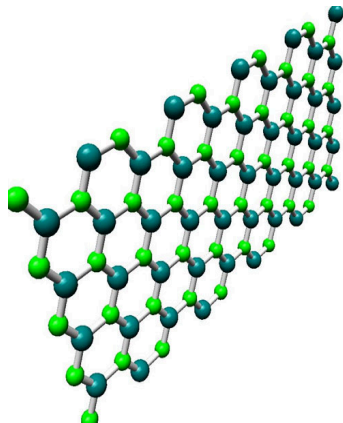
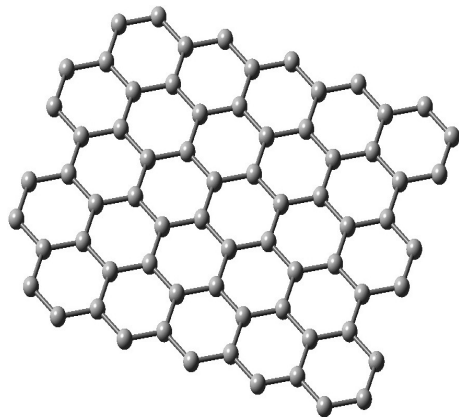
## Lattice structures

- Lattice structures are abundant in man-made and natural systems at various length scales
- Lattice structures are made of periodic identical/near-identical geometric units
- Among various lattice geometries (triangle, square, rectangle, pentagon, hexagon), hexagonal lattice is most common (note that hexagon is the highest “space filling” pattern in 2D).
- This talk is about in-plane elastic properties of 2D hexagonal lattice structures - commonly known as “honeycombs”



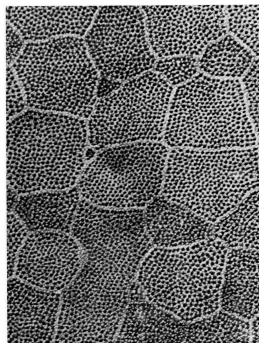
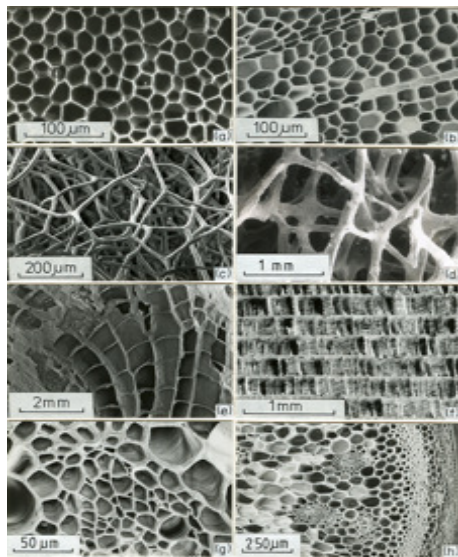
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# Lattice structures - nano scale



Single layer graphene sheet and boron nitride nano sheet

# Lattice structures - nature



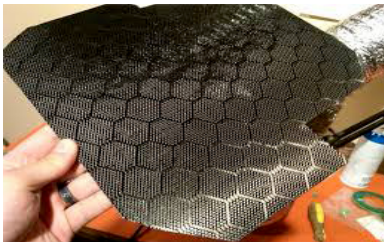
Top left: cork, top right: balsa, next down left: sponge, next down right: trabecular bone, next down left: coral, next down right: cuttlefish bone, bottom left: leaf tissue, bottom right: plant stem, third column - epidermal cells (from web.mit.edu)



# Lattice structures - man made



(a) Automotive: BMW i3



(b) Aerospace carbon fibre



(c) Civil engineering: building frame



(d) Architecture



## Some questions of general interest

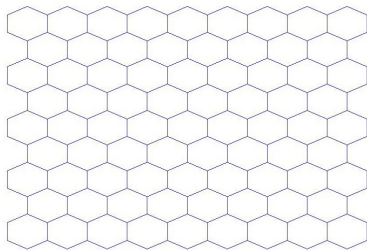
- Shall we consider lattices as “structures” or “materials” from a mechanics point of view?
- At what relative length-scale a lattice *structure* can be considered as a *material* with equivalent elastic properties?
- In what ways structural irregularities “mess up” equivalent elastic properties? Can we evaluate it in a quantitative as well as in a qualitative manner?
- What is the consequence of *random* structural irregularities on the homogenisation approach in general? Can we obtain statistical measures?
- Is there any underlying *ergodic* behaviour for “large” random lattices so that ensemble statistics is close to a sample statistics? How large is “large”?
- How can we efficiently *compute* equivalent elastic properties of random lattice structures?

## Regular lattice structures

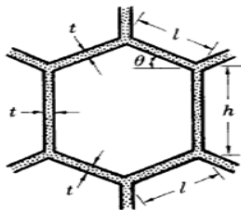
- Honeycombs have been modelled as a **continuous solid** with an equivalent elastic moduli throughout its domain.
- This approach **eliminates** the need of detail finite element modelling of honeycombs in complex structural systems like sandwich structures.
- Extensive amount of research has been carried out to predict the **equivalent elastic properties** of regular honeycombs consisting of perfectly periodic hexagonal cells (El-Sayed et al., 1979; Gibson and Ashby, 1999; Goswami, 2006; Masters and Evans, 1996; Zhang and Ashby, 1992).
- Analysis of two dimensional honeycombs dealing with **in-plane elastic properties** are commonly based on unit cell approach, which is applicable only for perfectly periodic cellular structures.

## Equivalent elastic properties of regular honeycombs

- Unit cell approach - Gibson and Ashby (1999)



(e) Regular hexagon ( $\theta = 30^\circ$ )



(f) Unit cell

- We are interested in homogenised equivalent in-plane elastic properties
- This way, we can avoid a detailed structural analysis considering all the beams and treat it as a material

## Equivalent elastic properties of regular honeycombs

- The cell walls are treated as beams of thickness  $t$ , depth  $b$  and Young's modulus  $E_s$ .  $l$  and  $h$  are the lengths of inclined cell walls having inclination angle  $\theta$  and the vertical cell walls respectively.
- The equivalent elastic properties are:

$$E_1 = E_s \left( \frac{t}{l} \right)^3 \frac{\cos \theta}{\left( \frac{h}{l} + \sin \theta \right) \sin^2 \theta} \quad (1)$$

$$E_2 = E_s \left( \frac{t}{l} \right)^3 \frac{\left( \frac{h}{l} + \sin \theta \right)}{\cos^3 \theta} \quad (2)$$

$$\nu_{12} = \frac{\cos^2 \theta}{\left( \frac{h}{l} + \sin \theta \right) \sin \theta} \quad (3)$$

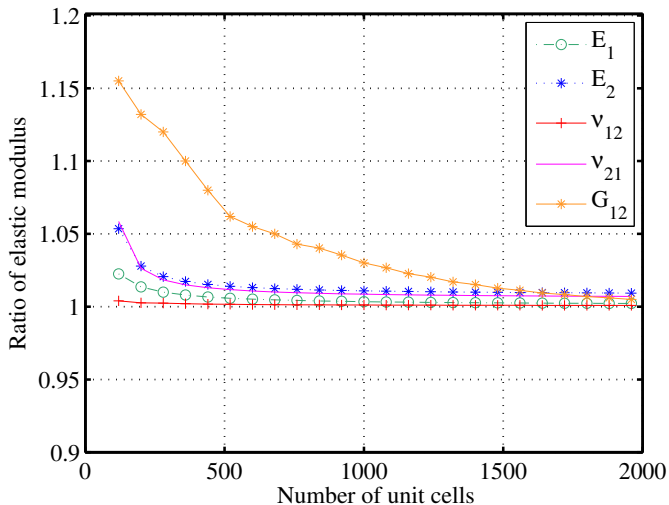
$$\nu_{21} = \frac{\left( \frac{h}{l} + \sin \theta \right) \sin \theta}{\cos^2 \theta} \quad (4)$$

$$G_{12} = E_s \left( \frac{t}{l} \right)^3 \frac{\left( \frac{h}{l} + \sin \theta \right)}{\left( \frac{h}{l} \right)^2 \left( 1 + 2 \frac{h}{l} \right) \cos \theta} \quad (5)$$

## Finite element modelling and verification

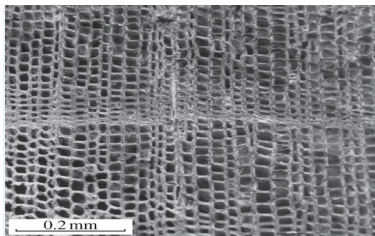
- A finite element code has been developed to obtain the in-plane elastic moduli numerically for honeycombs.
- Each cell wall has been modelled as an Euler-Bernoulli beam element having three degrees of freedom at each node.
- For  $E_1$  and  $\nu_{12}$ : two opposite edges parallel to direction-2 of the entire honeycomb structure are considered. Along one of these two edges, uniform stress parallel to direction-1 is applied while the opposite edge is restrained against translation in direction-1. Remaining two edges (parallel to direction-1) are kept free.
- For  $E_2$  and  $\nu_{21}$ : two opposite edges parallel to direction-1 of the entire honeycomb structure are considered. Along one of these two edges, uniform stress parallel to direction-2 is applied while the opposite edge is restrained against translation in direction-2. Remaining two edges (parallel to direction-2) are kept free.
- For  $G_{12}$ : uniform shear stress is applied along one edge keeping the opposite edge restrained against translation in direction-1 and 2, while the remaining two edges are kept free.

# Finite element modelling and verification



$\theta = 30^\circ$ ,  $h/l = 1.5$ . FE results converge to analytical predictions after 1681 cells.

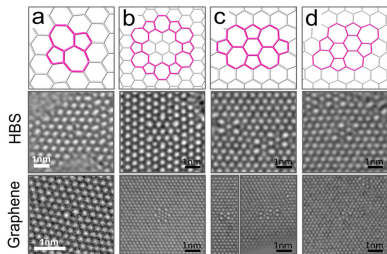
# Irregular lattice structures



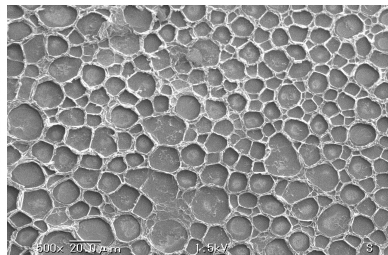
(g) Cedar wood



(h) Manufactured honeycomb core



(i) Graphene image



(j) Fabricated CNT surface

## Irregular lattice structures

- A **significant limitation** of the aforementioned unit cell approach is that it cannot account for the spatial irregularity, which is practically inevitable.
- **Spatial irregularity** in honeycomb may occur due to manufacturing uncertainty, structural defects, variation in temperature, pre-stressing and micro-structural variability in honeycombs.
- To include the effect of irregularity, **voronoi honeycombs** have been considered in several studies (Li et al., 2005; Zhu et al., 2001, 2006).
- The effect of different forms of irregularity on elastic properties and structural responses of honeycombs are generally based on **direct finite element (FE) simulation**.
- In the FE approach, a small change in geometry of a single cell may require completely new geometry and meshing of the entire structure. In general this makes the entire process **time-consuming and tedious**.
- The problem becomes even worse for **uncertainty quantification** of the responses associated with irregular honeycombs, where the expensive finite element model is needed to be simulated for a large number of samples while using a Monte Carlo based approach.

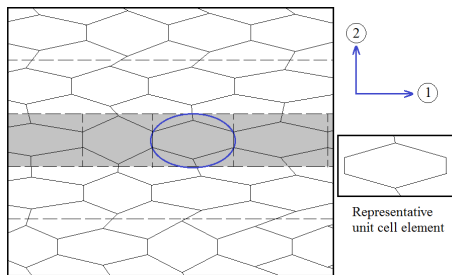


## Irregular lattice structures

- Direct numerical simulation to deal with irregularity in honeycombs may not necessarily provide proper understanding of the underlying physics of the system. An **analytical approach** could be a simple, insightful, yet an efficient way to obtain effective elastic properties of honeycombs.
- This work develops a structural mechanics based analytical framework for predicting equivalent in-plane elastic properties of irregular honeycomb having **spatially random** variations in cell angles.
- **Closed-form** analytical expressions will be derived for equivalent in-plane elastic properties.

## The philosophy of the analytical approach for irregular honeycombs

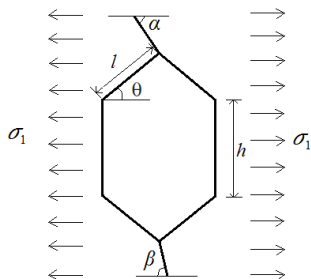
- The key idea to obtain the effective in-plane elastic moduli of the entire irregular honeycomb structure is that it is considered to be consisted of several **Representative Unit Cell Elements (RUCE)** having different individual elastic moduli.



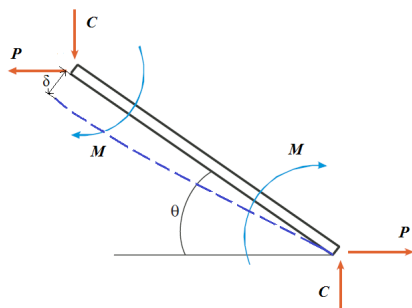
- The expressions for elastic moduli of a RUCE is derived first and subsequently the expressions for effective in-plane elastic moduli of the entire irregular honeycomb are derived by assembling the individual elastic moduli of these RUCEs using basic principles of mechanics (**divide and conquer!**).

## Longitudinal Young's modulus ( $E_1$ )

- To derive the expression of longitudinal Young's modulus for a RUCE ( $E_{1U}$ ), stress  $\sigma_1$  is applied in direction-1 as shown below:



(k)



(l)

**Figure:** RUCE and free-body diagram used in the analysis for  $E_1$

## Elastic property of a representative unit cell element (RUCE)

- The inclined cell walls having inclination angle  $\alpha$  and  $\beta$  do not have any contribution in the analysis, as the stresses applied on them in two opposite directions neutralise each other. The remaining structure except these two inclined cell walls is symmetric.
- The applied stresses cause the inclined cell walls having inclination angle  $\theta$  to bend.
- From the condition of equilibrium, the vertical forces  $C$  in the free-body diagram of these cell walls need to be zero. The cell walls are treated as beams of thickness  $t$ , depth  $b$  and Young's modulus  $E_s$ .  $l$  and  $h$  are the lengths of inclined cell walls having inclination angle  $\theta$  and the vertical cell walls respectively.
- Therefore, we have

$$M = \frac{Pl \sin \theta}{2} \quad (6)$$

where

$$P = \sigma_1(h + l \sin \theta)b \quad (7)$$

## Elastic property of a representative unit cell element (RUCE)

- From the standard beam theory, the deflection of one end compared to the other end of the cell wall can be expressed as

$$\delta = \frac{Pl^3 \sin \theta}{12E_s l} \quad (8)$$

where  $l$  is the second moment of inertia of the cell wall, that is  $l = bt^3/12$ .

- The component of  $\delta$  parallel to direction-1 is  $\delta \sin \theta$ . The strain parallel to direction-1 becomes

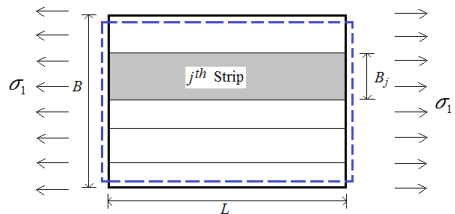
$$\epsilon_1 = \frac{\delta \sin \theta}{l \cos \theta} \quad (9)$$

Thus the Young's modulus in direction-1 for a RUCE can be expressed as

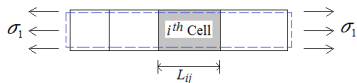
$$E_{1U} = \frac{\sigma_1}{\epsilon_1} = E_s \left( \frac{t}{l} \right)^3 \frac{\cos \theta}{\left( \frac{h}{l} + \sin \theta \right) \sin^2 \theta} \quad (10)$$

- Next we use this to obtain  $E_1$  for the entire structure.

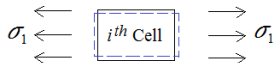
## Elastic property of the entire irregular honeycomb



(a) Entire idealized irregular honeycomb structure



(b) Idealized  $j^{\text{th}}$  strip



(c) Idealized  $i^{\text{th}}$  cell in  $j^{\text{th}}$  strip

**Figure:** Free-body diagrams of idealized irregular honeycomb structure in the proposed analysis of  $E_1$

- The entire irregular honeycomb structure is assumed to have  $m$  and  $n$  number of RUCs in direction-1 and direction-2 respectively. A particular cell having position at  $i^{\text{th}}$  column and  $j^{\text{th}}$  row is represented as  $(i,j)$ , where  $i = 1, 2, \dots, m$  and  $j = 1, 2, \dots, n$ .

## Elastic property of the entire irregular honeycomb

- To obtain  $E_{1eq}$ , stress  $\sigma_1$  is applied in direction-1. If the deformation compatibility condition of  $j^{th}$  strip (as highlighted in the figure) is considered, the **total deformation** due to stress  $\sigma_1$  of that particular strip ( $\Delta_1$ ) is the **summation** of individual deformations of each RUCs in direction-1, while deformation of each of these RUCs in direction-2 is the same.
- Thus for the  $j^{th}$  strip

$$\Delta_1 = \sum_{i=1}^m \Delta_{1ij} \quad (11)$$

The equation (11) can be rewritten as

$$\epsilon_1 L = \sum_{i=1}^m \epsilon_{1ij} L_{ij} \quad (12)$$

where  $\epsilon_1$  and  $L$  represent strain and dimension in direction-1 of respective elements.

## Elastic property of the entire irregular honeycomb

- Equation (12) leads to

$$\frac{\sigma_1 L}{\hat{E}_{1j}} = \sum_{i=1}^m \frac{\sigma_1 L_{ij}}{E_1 U_{ij}} \quad (13)$$

- From equation (13), equivalent Young's modulus of  $j^{\text{th}}$  strip ( $\hat{E}_{1j}$ ) can be expressed as

$$\hat{E}_{1j} = \frac{\sum_{i=1}^m l_{ij} \cos \theta_{ij}}{\sum_{i=1}^m \frac{l_{ij} \cos \theta_{ij}}{E_1 U_{ij}}} \quad (14)$$

where  $\theta_{ij}$  is the inclination angle of the cell walls having length  $l_{ij}$  in the RUC positioned at  $(i,j)$ .



## Elastic property of the entire irregular honeycomb

- After obtaining the Young's moduli of  $n$  number of strips, they are assembled to achieve the equivalent Young's modulus of the entire irregular honeycomb structure ( $E_{1eq}$ ) using **force equilibrium** and **deformation compatibility** conditions.

$$\sigma_1 B b = \sum_{j=1}^n \sigma_{1j} B_j b \quad (15)$$

where  $B_j$  is the dimension of  $j^{th}$  strip in direction-2 and  $B = \sum_{j=1}^n B_j$ .  $b$  represents the depth of honeycomb.

- As strains in direction-1 for each of the  $n$  strips are same to satisfy the deformation compatibility condition, equation (15) leads to

$$\left( \sum_{j=1}^n B_j \right) E_{1eq} = \sum_{j=1}^n \hat{E}_{1j} B_j \quad (16)$$

## Elastic property of the entire irregular honeycomb

- Using equation (14) and equation (16), equivalent Young's modulus in direction-1 of the entire irregular honeycomb structure ( $E_{1eq}$ ) can be expressed as:

### Equivalent $E_1$

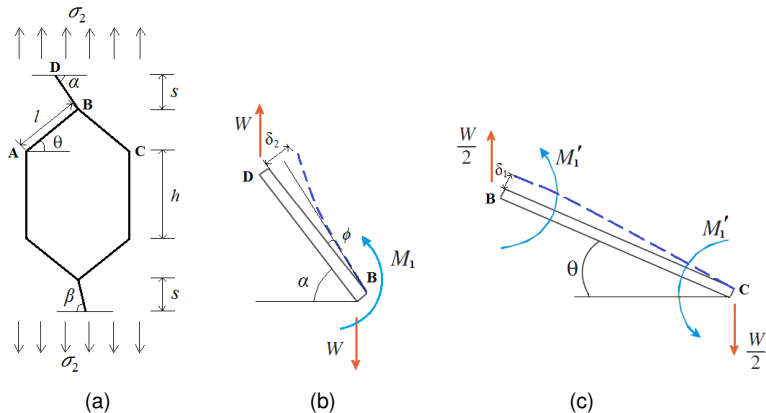
$$E_{1eq} = \frac{1}{\sum_{j=1}^n B_j} \sum_{j=1}^n \left( \frac{\sum_{i=1}^m l_{ij} \cos \theta_{ij}}{\sum_{i=1}^m \frac{l_{ij} \cos \theta_{ij}}{E_{1Uij}}} \right) B_j \quad (17)$$

- Here Young's modulus in direction-1 of a RUCE positioned at  $(i,j)$  is  $E_{1Uij}$ , which can be obtained from equation (10) as

$$E_{1Uij} = E_s \left( \frac{t}{l_{ij}} \right)^3 \frac{\cos \theta_{ij}}{\left( \frac{h}{l_{ij}} + \sin \theta_{ij} \right) \sin^2 \theta_{ij}} \quad (18)$$

## Transverse Young's modulus ( $E_2$ )

- To derive the expression of transverse Young's modulus for a RUCE ( $E_{2U}$ ), stress  $\sigma_2$  is applied in direction-2 as shown below:



**Figure:** RUCE and free-body diagram used in the proposed analysis for  $E_2$

## Elastic property of a representative unit cell element (RUCE)

- Total deformation of the RUCE in direction-2 consists of three components, namely deformation of the cell wall having inclination angle  $\alpha$ , deformation of the cell walls having inclination angle  $\theta$  and deformation of the cell wall having inclination angle  $\beta$ .
- If the remaining structure except the two inclined cell walls having inclination angle  $\alpha$  and  $\beta$  is considered, two forces that act at joint B are  $W$  and  $M_1$ . For the cell wall having inclination angle  $\alpha$ , effect of the bending moment  $M_1$  generated due to application of  $W$  at point D is only to create rotation ( $\phi$ ) at the joint B.
- Vertical deformation of the cell wall having inclination angle  $\alpha$  has two components, bending deformation in direction-2 and rotational deformation due the rotation of joint B.

## Elastic property of a representative unit cell element (RUCE)

- After some algebra and mechanics, the total deformation in direction-2 of the RUCE due to the application of stresses  $\sigma_2$  is

$$\delta_v = \frac{\sigma_2 l \cos \theta}{E_s t^3} \left( 2l^3 \cos^2 \theta + 8s^3 \left( \frac{\cos^2 \alpha}{\sin^3 \alpha} + \frac{\cos^2 \beta}{\sin^3 \beta} \right) + 2s^2 l (\cot^2 \alpha + \cot^2 \beta) \right) \quad (19)$$

- The strain in direction-2 can be obtained as

$$\epsilon_2 = \frac{\delta_v}{h + 2s + 2l \sin \theta} \quad (20)$$

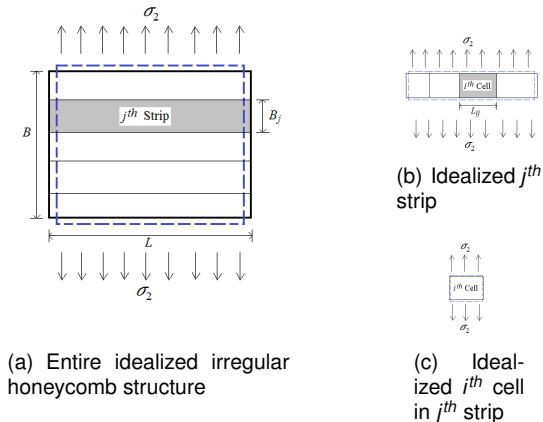
## Elastic property of a representative unit cell element (RUCE)

- Therefore, the Young's modulus in direction-2 of a RUCE can be expressed as

$$E_{2U} = \frac{\sigma_2}{\epsilon_2} = E_s \left(\frac{t}{l}\right)^3 \times \frac{\left(\frac{h}{l} + 2\frac{s}{l} + 2\sin\theta\right)}{\cos\theta \left(2\cos^2\theta + 8\left(\frac{s}{l}\right)^3 \left(\frac{\cos^2\alpha}{\sin^3\alpha} + \frac{\cos^2\beta}{\sin^3\beta}\right) + 2\left(\frac{s}{l}\right)^2 (\cot^2\alpha + \cot^2\beta)\right)} \quad (21)$$

## Elastic property of the entire irregular honeycomb

- To derive the expression of equivalent Young's modulus in direction-2 for the entire irregular honeycomb structure ( $E_{2eq}$ ), the Young's moduli for the constituting RUCs ( $E_{2U}$ ) are "assembled".



**Figure:** Free-body diagrams of idealized irregular honeycomb structure

## Elastic property of the entire irregular honeycomb

- When the force equilibrium under the application of stress  $\sigma_2$  of  $j^{\text{th}}$  strip (as highlighted in 4(b)) is considered:

$$\sigma_2 \left( \sum_{i=1}^m 2l_{ij} \cos \theta_{ij} \right) b = \left( \sum_{i=1}^m \sigma_{2ij} 2l_{ij} \cos \theta_{ij} \right) b \quad (22)$$

- By deformation compatibility condition, strains of each RUCE in direction-2 of the  $j^{\text{th}}$  strip are same. Equation (22), rewritten as

$$\hat{E}_{2j} \left( \sum_{i=1}^m l_{ij} \cos \theta_{ij} \right) \epsilon = \left( \sum_{i=1}^m E_{2Uij} l_{ij} \cos \theta_{ij} \epsilon_{ij} \right) \quad (23)$$

where  $\epsilon_{ij} = \epsilon$ , for  $i = 1, 2 \dots m$  in the  $j^{\text{th}}$  strip.

- $\hat{E}_{2j}$  is the equivalent elastic modulus in direction-2 of the  $j^{\text{th}}$  strip:

$$\hat{E}_{2j} = \frac{\sum_{i=1}^m E_{2Uij} l_{ij} \cos \theta_{ij}}{\sum_{i=1}^m l_{ij} \cos \theta_{ij}} \quad (24)$$



## Elastic property of the entire irregular honeycomb

- Total deformation of the entire honeycomb in direction-2 ( $\Delta_2$ ) is the sum of deformations of each strips in that direction,

$$\Delta_2 = \sum_{j=1}^n \Delta_{2ij} \quad (25)$$

- Equation (25) can be rewritten as

$$\epsilon_2 B = \sum_{j=1}^n \epsilon_{2j} B_j \quad (26)$$

where  $\epsilon_2$ ,  $\epsilon_{2j}$  and  $B_j$  represent total strain of the entire honeycomb structure in direction-2, strain of  $j^{\text{th}}$  strip in direction-2 and dimension in direction-2 of  $j^{\text{th}}$  strip respectively.

- From equation (26) we have

$$\frac{\sigma_2 \sum_{j=1}^n B_j}{E_{2eq}} = \sum_{j=1}^n \frac{\sigma_2 B_j}{\hat{E}_{2j}} \quad (27)$$

## Elastic property of the entire irregular honeycomb

- From equation (24) and equation (27), the Young's modulus in direction-2 of the entire irregular honeycomb structure can be expressed as

### Equivalent $E_2$

$$E_{2eq} = \frac{1}{\left( \frac{\sum_{j=1}^n B_j \frac{\sum_{i=1}^m l_{ij} \cos \theta_{ij}}{\sum_{i=1}^m E_{2Uij} l_{ij} \cos \theta_{ij}}}{\sum_{j=1}^n B_j} \right)} \sum_{j=1}^n B_j \quad (28)$$

- Here Young's modulus in direction-2 of a RUCE positioned at  $(i,j)$  is  $E_{2Uij}$ , which can be obtained from equation (21).

## Special case: classical deterministic results

- The expressions of Young's moduli for randomly irregular honeycombs (equation (17) and (28)) reduces to the formulae provided by Gibson and Ashby (Gibson and Ashby, 1999) in case of uniform honeycombs (i.e.  $B_1 = B_2 = \dots = B_n$ ;  $s = h/2$ ;  $\alpha = \beta = 90^\circ$ ;  $l_{ij} = l$  and  $\theta_{ij} = \theta$ , for all  $i$  and  $j$ ).
- By applying the conditions  $B_1 = B_2 = \dots = B_n$ ;  $l_{ij} = l$  and  $\theta_{ij} = \theta$ , equation (17) and (28) reduce to  $E_{1U}$  and  $E_{2U}$  respectively.
- For  $s = h/2$  and  $\alpha = \beta = 90^\circ$ ,  $E_{1U}$  and  $E_{2U}$  produce the same expressions for Young's moduli of uniform honeycomb as presented by Gibson and Ashby (Gibson and Ashby, 1999).
- In the case of regular uniform honeycombs ( $\theta = 30^\circ$ )

$$\frac{E_1^*}{E_s} = \frac{E_2^*}{E_s} = 2.3 \left( \frac{t}{l} \right)^3 \quad (29)$$

where  $E_1^*$  and  $E_2^*$  denote the Young moduli of uniform regular honeycombs in longitudinal and transverse direction respectively.

## Poisson's ratio $\nu_{12}$

- Poisson's ratios are calculated by taking the negative ratio of strains normal to, and parallel to, the loading direction.
- Poisson's ratio of a RUCE for the loading direction-1 ( $\nu_{12U}$ ) is obtained as

$$\nu_{12U} = -\frac{\epsilon_2}{\epsilon_1} \quad (30)$$

where  $\epsilon_1$  and  $\epsilon_2$  represent the strains of a RUCE in direction-1 and direction-2 respectively due to loading in direction-1.

- $\epsilon_1$  can be obtained from equation (9). From 1(l),  $\epsilon_2$  can be expressed as

$$\epsilon_2 = -\frac{2\delta \cos \theta}{h + 2l \sin \theta + 2s} \quad (31)$$

- Thus the expression for Poisson's ratio of a RUCE for the loading direction-1 becomes

$$\nu_{12U} = \frac{2 \cos^2 \theta}{\left(2 \sin \theta + 2 \frac{s}{l} + \frac{h}{l}\right) \sin \theta} \quad (32)$$

## Poisson's ratio of the entire irregular honeycomb

- To derive the expression of equivalent Poisson's ratio for loading direction-1 of the entire irregular honeycomb structure ( $\nu_{12eq}$ ), the Poisson's ratios for the constituting RUCs ( $\nu_{12U}$ ) are "assembled".
- For obtaining  $\nu_{12eq}$ , stress  $\sigma_1$  is applied in direction-1. If the application of stress  $\sigma_1$  in the  $j^{th}$  strip is considered, total deformation of the  $j^{th}$  strip in direction-1 is summation of individual deformations of the RUCs in direction-1 of that particular strip.
- Thus from equation (12), using the basic definition of  $\nu_{12}$ ,

$$-\frac{\epsilon_2}{\hat{\nu}_{12j}} L = -\sum_{i=1}^m \frac{\epsilon_{2ij} L_{ij}}{\nu_{U12ij}} \quad (33)$$

where  $\epsilon_2$  and  $\epsilon_{2ij}$  are the strains in direction-2 of  $j^{th}$  strip and individual RUCs of  $j^{th}$  strip respectively.

- $\nu_{U12ij}$  represents the Poisson's ratio for loading direction-1 of a RUC positioned at  $(i,j)$ .  $\hat{\nu}_{12j}$  denotes the equivalent Poisson's ratio for loading direction-1 of the  $j^{th}$  strip.

## Poisson's ratio of the entire irregular honeycomb

- Ensuring the deformation compatibility condition  $\epsilon_2 = \epsilon_{2ij}$  for  $i = 1, 2, \dots, m$  in the  $j^{\text{th}}$  strip, equation (33) leads to

$$\hat{\nu}_{12j} = \frac{L}{\sum_{i=1}^m \frac{L_{ij}}{\nu_{12} U_{ij}}} \quad (34)$$

- Total deformation of the entire honeycomb structure in direction-2 under the application of stress  $\sigma_1$  along the two opposite edges parallel to direction-2 is summation of the individual deformations in direction-2 of  $n$  number of strips. Thus

$$\epsilon_2 B = \sum_{j=1}^n \epsilon_{2j} B_j \quad (35)$$

## Poisson's ratio of the entire irregular honeycomb

- Using the basic definition of  $\nu_{12}$  equation (35) becomes

$$\nu_{12eq}\epsilon_1 B = \sum_{j=1}^n \nu_{12j}\epsilon_{1j} B_j \quad (36)$$

where  $\nu_{12eq}$  represents the equivalent Poisson's ratio for loading direction-1 of the entire irregular honeycomb structure.

- $\epsilon_1$  and  $\epsilon_{1j}$  denote the strain of entire honeycomb structure in direction-1 and strain of  $j^{th}$  strip in direction-1 respectively.
- From the condition of deformation comparability  $\epsilon_1 = \epsilon_{1j}$  for  $j = 1, 2, \dots, n$ . Thus from equation (34) and equation (36):

### Equivalent $\nu_{12}$

$$\nu_{12eq} = \frac{1}{\sum_{j=1}^n B_j} \sum_{j=1}^n \left( \frac{\sum_{i=1}^m l_{ij} \cos \theta_{ij}}{\sum_{i=1}^m \frac{l_{ij} \cos \theta_{ij}}{\nu_{12Uij}}} \right) B_j \quad (37)$$

Here  $\nu_{12Uij}$  can be obtained from equation (32).

## Poisson's ratio $\nu_{21}$

- Poisson's ratio of a RUCE for the loading direction-2 ( $\nu_{21U}$ ) is obtained as

$$\nu_{21U} = -\frac{\epsilon_1}{\epsilon_2} \quad (38)$$

where  $\epsilon_1$  and  $\epsilon_2$  represent the strains of a RUCE in direction-1 and direction-2 respectively due to loading in direction-2.

- $\epsilon_2$  can be obtained from equation (19) and equation (20) as

$$\epsilon_2 = \frac{\sigma_2 l \cos \theta}{E_s t^3 (h + 2s + 2l \sin \theta)} \left( 2l^3 \cos^2 \theta + 8s^3 \left( \frac{\cos^2 \alpha}{\sin^3 \alpha} + \frac{\cos^2 \beta}{\sin^3 \beta} \right) + 2s^2 l (\cot^2 \alpha + \cot^2 \beta) \right) \quad (39)$$

- We have

$$\epsilon_1 = -\frac{\delta_1 \sin \theta}{l \cos \theta} \quad (40)$$

$$\text{with } \delta_1 = \frac{\left( \frac{W}{2} \cos \theta \right) l^3}{12E_s l} \text{ and } W = 2\sigma_2 l b \cos \theta.$$



## Poisson's ratio of a representative unit cell element (RUCE)

- Thus equation (40) reduces to

$$\epsilon_1 = -\frac{\sigma_2 l^3 \sin \theta \cos \theta}{E_s t^3} \quad (41)$$

- Thus the expression for Poisson's ratio of a RUCE for the loading direction-2 becomes

$$\nu_{21U} = \frac{\sin \theta \left( \frac{h}{l} + 2 \frac{s}{l} + 2 \sin \theta \right)}{2 \cos^2 \theta + 8 \left( \frac{s}{l} \right)^3 \left( \frac{\cos^2 \alpha}{\sin^3 \alpha} + \frac{\cos^2 \beta}{\sin^3 \beta} \right) + 2 \left( \frac{s}{l} \right)^2 (\cot^2 \alpha + \cot^2 \beta)} \quad (42)$$

## Poisson's ratio of the entire irregular honeycomb

- To derive the expression of equivalent Poisson's ratio for loading direction-2 of the entire irregular honeycomb structure ( $\nu_{21eq}$ ), the Poisson's ratios for the constituting RUCs ( $\nu_{21U}$ ) are assembled.
- For obtaining  $\nu_{21eq}$ , stress  $\sigma_2$  is applied in direction-2. If the application of stress  $\sigma_2$  in the  $j^{th}$  strip is considered, total deformation of the  $j^{th}$  strip in direction-1 is summation of individual deformations of the RUCs in direction-1 of that particular strip. Thus,

$$\epsilon_1 L = \sum_{i=1}^m \epsilon_{1ij} L_{ij} \quad (43)$$

- Using the basic definition of  $\nu_{21}$  equation (43) leads to

$$\hat{\nu}_{21j} \epsilon_2 L = \sum_{i=1}^m \nu_{21Uij} \epsilon_{2ij} L_{ij} \quad (44)$$

where  $\hat{\nu}_{21j}$  represents the equivalent Poisson's ratio for loading direction-2 of the  $j^{th}$  strip.

## Poisson's ratio of the entire irregular honeycomb

- $\epsilon_2$  and  $\epsilon_{2ij}$  are the strains in direction-2 of  $j^{\text{th}}$  strip and individual RUCs of  $j^{\text{th}}$  strip respectively.  $\nu_{21Uij}$  represents the Poisson's ratio for loading direction-2 of a RUC positioned at  $(i,j)$ .
- To ensure the deformation compatibility condition  $\epsilon_2 = \epsilon_{2ij}$  for  $i = 1, 2, \dots, m$  in the  $j^{\text{th}}$  strip. Thus equation (44) leads to

$$\nu_{21j}^{\hat{}} = \frac{\sum_{i=1}^m \nu_{21Uij} l_{ij} \cos \theta_{ij}}{\sum_{i=1}^m l_{ij} \cos \theta_{ij}} \quad (45)$$

- Total deformation of the entire honeycomb structure in direction-2 under the application of stress  $\sigma_2$  along the two opposite edges parallel to direction-1 is summation of the individual deformations in direction-2 of  $n$  number of strips. Thus

$$\epsilon_2 B = \sum_{j=1}^n \epsilon_{2j} B_j \quad (46)$$

## Poisson's ratio of the entire irregular honeycomb

- By definition of  $\nu_{21}$  equation (46) leads to

$$\frac{\epsilon_1}{\nu_{21eq}} B = \sum_{j=1}^n \frac{\epsilon_{1j}}{\hat{\nu}_{21j}} B_j \quad (47)$$

- From the condition of deformation comparability  $\epsilon_1 = \epsilon_{1j}$  for  $j = 1, 2, \dots, n$ . Thus the equivalent Poisson's ratio for loading direction-2 of the entire irregular honeycomb structure:

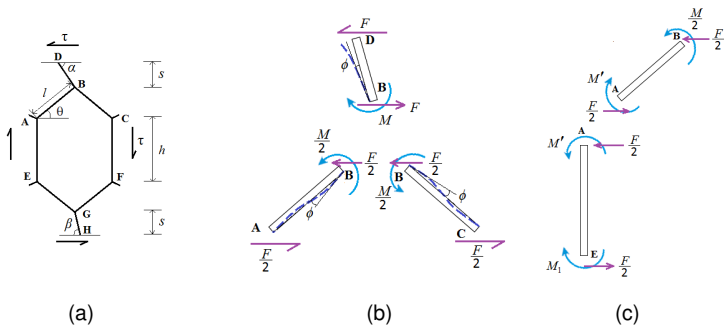
### Equivalent $\nu_{12}$

$$\nu_{21eq} = \frac{1}{\left( \frac{\sum_{j=1}^n B_j \frac{\sum_{i=1}^m l_{ij} \cos \theta_{ij}}{\sum_{i=1}^m \nu_{21Uij} l_{ij} \cos \theta_{ij}}}{\sum_{j=1}^n B_j} \right)} \sum_{j=1}^n B_j \quad (48)$$

Here  $\nu_{21Uij}$  can be obtained from equation (42).

## Shear modulus ( $G_{12}$ )

- To derive the expression of shear modulus ( $G_{12U}$ ) for a RUCE, shear stress  $\tau$  is applied as shown below:



**Figure:** RUCE and free-body diagram used in the proposed analysis for  $G_{12}$

## Elastic property of a representative unit cell element (RUCE)

- Total lateral movement of point D with respect to point H can be obtained as

$$\delta_L = \frac{2\tau l \cos \theta}{Et^3} \left( 2ls^2 + \frac{h^3}{2} + 4s^3 \left( \frac{1}{\sin \alpha} + \frac{1}{\sin \beta} \right) + (s + l \sin \theta)h^2 \right) \quad (49)$$

- The shear strain  $\gamma$  for a RUCE can be expressed as

$$\gamma = \frac{\delta_L}{2s + h + 2l \sin \theta} = \frac{2\tau l \cos \theta}{Et^3(2s + h + 2l \sin \theta)} \times \left( 2ls^2 + \frac{h^3}{2} + 4s^3 \left( \frac{1}{\sin \alpha} + \frac{1}{\sin \beta} \right) + (s + l \sin \theta)h^2 \right) \quad (50)$$

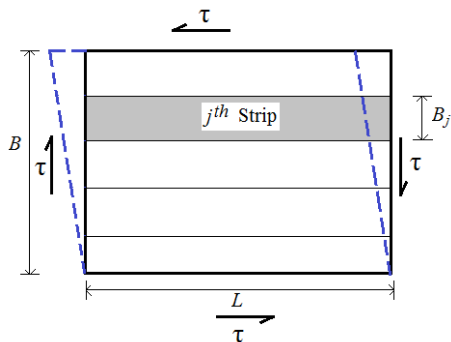
## Elastic property of a representative unit cell element (RUCE)

- Thus the expression for shear modulus of a RUCE becomes

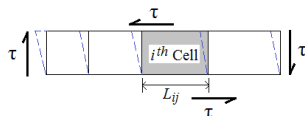
$$G_{12U} = \frac{\tau}{\gamma} = E_s \left( \frac{t}{l} \right)^3 \times \frac{\left( 2 \frac{s}{l} + \frac{h}{l} + 2 \sin \theta \right)}{2 \cos \theta \left( 2 \left( \frac{s}{l} \right)^2 + 4 \left( \frac{s}{l} \right)^3 \left( \frac{1}{\sin \alpha} + \frac{1}{\sin \beta} \right) + \frac{1}{2} \left( \frac{h}{l} \right)^3 + \left( \frac{s}{l} + \sin \theta \right) \left( \frac{h}{l} \right)^2 \right)} \quad (51)$$

## Elastic property of the entire irregular honeycomb

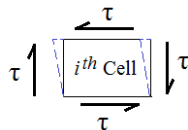
- To derive the expression of equivalent shear modulus of the entire irregular honeycomb structure ( $G_{12eq}$ ), the shear moduli for the constituting RUCs ( $G_{12U}$ ) are “assembled”:



(a) Entire idealized irregular honeycomb structure



(b) Idealized  $j^{\text{th}}$  strip



(c) Idealized  $i^{\text{th}}$  cell in  $j^{\text{th}}$  strip

**Figure:** Free-body diagrams of idealized irregular honeycomb structure in the proposed analysis of  $G_{12}$



## Elastic property of the entire irregular honeycomb

- For obtaining  $G_{12eq}$ , shear stress  $\tau$  is applied parallel to direction direction-1. If the equilibrium of forces for application of stress  $\tau$  in the  $j^{th}$  strip is considered:

$$\tau L = \sum_{i=1}^m \tau_{ij} L_{ij} \quad (52)$$

- By definition of shear modulus equation (52) can be rewritten as

$$\hat{G}_{12j} \gamma L = \sum_{i=1}^m G_{12Uij} \gamma_{ij} L_{ij} \quad (53)$$

where  $\hat{G}_{12j}$  represents the equivalent shear modulus of the  $j^{th}$  strip.

- $\gamma$  and  $\gamma_{ij}$  are the shear strains of  $j^{th}$  strip and individual RUCes of the  $j^{th}$  strip respectively.  $G_{12Uij}$  represents the shear modulus of a RUC positioned at  $(i,j)$ .

## Elastic property of the entire irregular honeycomb

- To ensure the deformation compatibility condition  $\gamma = \gamma_{ij}$  for  $i = 1, 2, \dots, m$  in the  $j^{\text{th}}$  strip. Thus equation (53) leads to

$$\hat{G}_{12j} = \frac{\sum_{i=1}^m G_{12Uij} l_{ij} \cos \theta_{ij}}{\sum_{i=1}^m l_{ij} \cos \theta_{ij}} \quad (54)$$

- Total lateral deformation of one edge compared to the opposite edge of the entire honeycomb structure under the application of shear stress  $\tau$  is the summation of the individual lateral deformations of  $n$  number of strips. Thus

$$\gamma B = \sum_{j=1}^n \gamma_j B_j \quad (55)$$

- By definition of  $G_{12}$  equation (55) leads to

$$\frac{\tau}{G_{12eq}} B = \sum_{j=1}^n \frac{\tau_j}{\hat{G}_{12j}} B_j \quad (56)$$

## Elastic property of the entire irregular honeycomb

- From equation (54) and (56), the equivalent shear modulus of the entire irregular honeycomb structure can be expressed as:

### Equivalent $G_{12}$

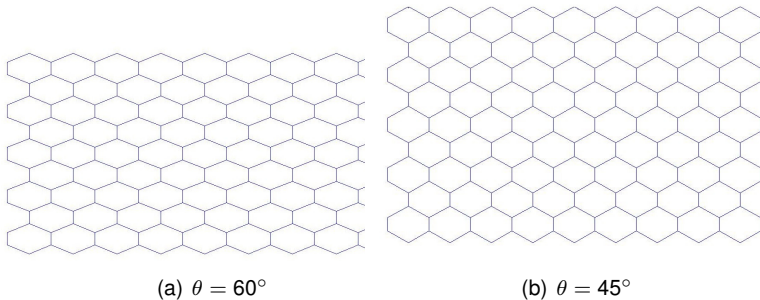
$$G_{12eq} = \frac{1}{\left( \frac{\sum_{j=1}^n B_j \frac{\sum_{i=1}^m l_{ij} \cos \theta_{ij}}{\sum_{i=1}^m G_{12Uij} l_{ij} \cos \theta_{ij}}}{\sum_{j=1}^n B_j} \right)} \sum_{j=1}^n B_j \quad (57)$$

Here  $G_{12Uij}$  can be obtained from equation (51).

## Computational model and validation

- The analytical approach is capable of obtaining equivalent in-plane elastic properties for irregular honeycombs from known random spatial variation of cell angle and material properties of the honeycomb cells.
- The homogenised properties depend on the ratios  $h/l$ ,  $t/l$ ,  $s/l$  and the angles  $\theta$ ,  $\alpha$ ,  $\beta$ . In addition, the two Young's moduli and shear modulus also depend on  $E_s$ .
- We show results for  $h/l = 1.5$  and three values of cell angle  $\theta$ , namely:  $30^\circ$ ,  $45^\circ$  and  $60^\circ$ .
- As the two Young's moduli and shear modulus of low density honeycomb are proportional to  $E_s \rho^3$  (Zhu et al., 2001), the non-dimensional results for elastic moduli  $E_1$ ,  $E_2$ ,  $\nu_{12}$ ,  $\nu_{21}$  and  $G_{12}$  have been obtained using  $\bar{E}_1 = \frac{E_{1eq}}{E_s \rho^3}$ ,  $\bar{E}_2 = \frac{E_{2eq}}{E_s \rho^3}$ ,  $\bar{\nu}_{12} = \nu_{12eq}$ ,  $\bar{\nu}_{21} = \nu_{21eq}$  and  $\bar{G}_{12} = \frac{G_{12eq}}{E_s \rho^3}$  respectively, where ' $\bar{\cdot}$ ' represents the non-dimensional elastic modulus and  $\rho$  is the relative density of honeycomb (ratio of the planar area of solid to the total planar area of the honeycomb).

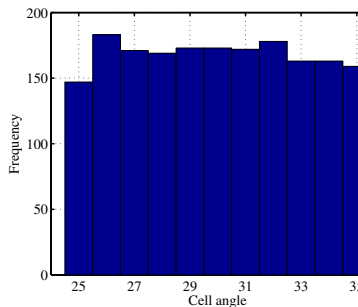
# Computational model and validation



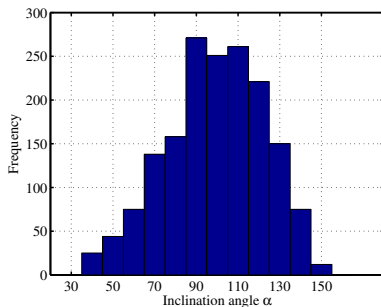
**Figure:** Regular honeycomb with different  $\theta$  values

## Computational model and validation

- For the purpose of finding the range of variation in elastic moduli due to spatial uncertainty, cell angles and material properties can be perturbed following a random distribution within specific bounds. We show results for **spatial irregularity in the cell angles only**.



(a) Distribution of cell angle ( $\theta$ )



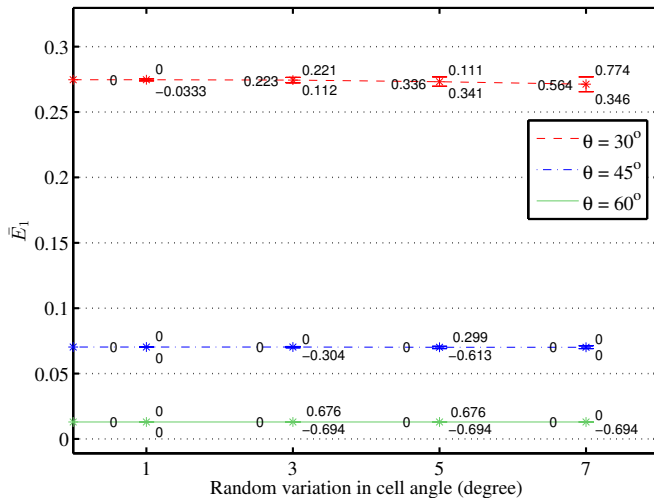
(b) Distribution of the inclination angle ( $\alpha$ )

**Figure:** Typical statistical distribution of cell angle ( $\theta$ ) and inclination angle  $\alpha$  (number of RUC: 1681)

## Computational model and validation

- The maximum, minimum and mean values of non-dimensional in-plane elastic moduli for different degree of spatially random variations in cell angles ( $\Delta\theta = 0^\circ, 1^\circ, 3^\circ, 5^\circ, 7^\circ$ ) are calculated using both direct finite element simulation and the derived closed-form expressions.
- For a particular cell angle  $\theta$ , results have been obtained using a set of uniformly distributed 1000 random samples in the range of  $[\theta - \Delta\theta, \theta + \Delta\theta]$ .
- The set of input parameter for a particular sample consists of  $N$  number of cell angles in the specified range, where  $N(= n \times m)$  is the total number of RUCs in the entire irregular honeycomb structure. We used 1681 RUCs (as this was needed for convergence of the deterministic case).
- The quantities  $h$  and  $\theta$  have been considered as the two random input parameters while  $\alpha$ ,  $\beta$  and  $l$  are dependent features.

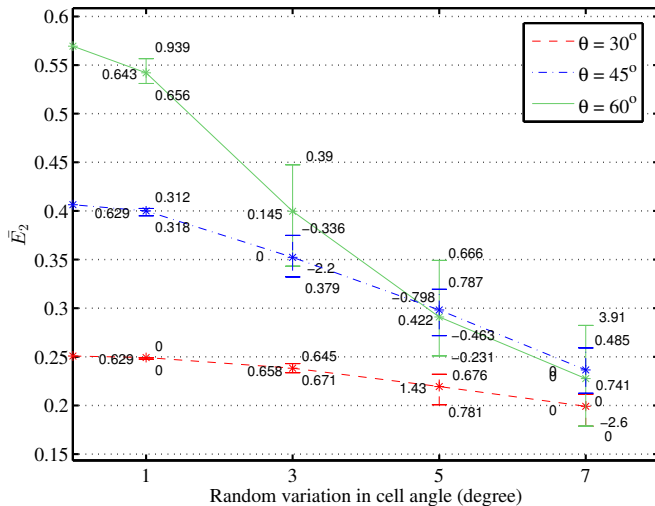
# Longitudinal elastic modulus ( $E_1$ )



$$h/l = 1.5, \bar{E}_1 = E_{1eq}/E_s\rho^3$$

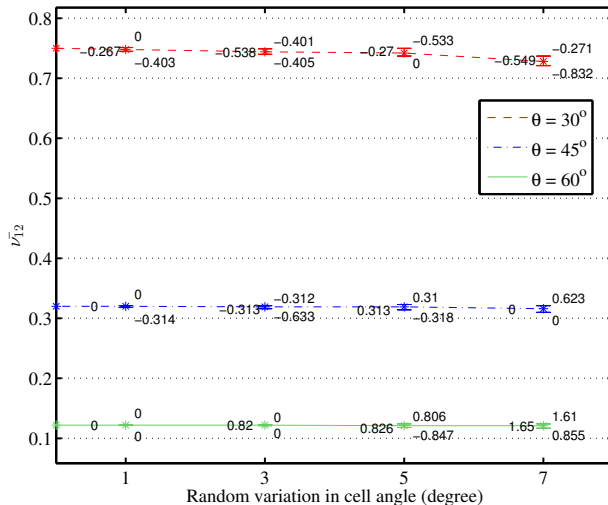


# Transverse elastic modulus ( $E_2$ )



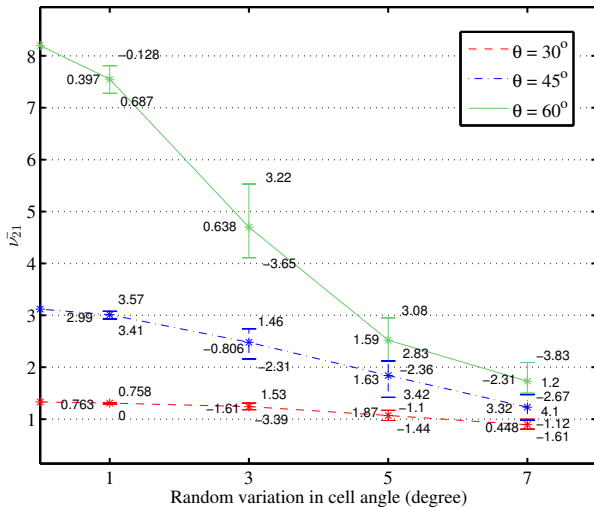
$$h/l = 1.5, \bar{E}_2 = E_{2eq}/E_s\rho^3$$

# Poisson's ratio $\nu_{12}$

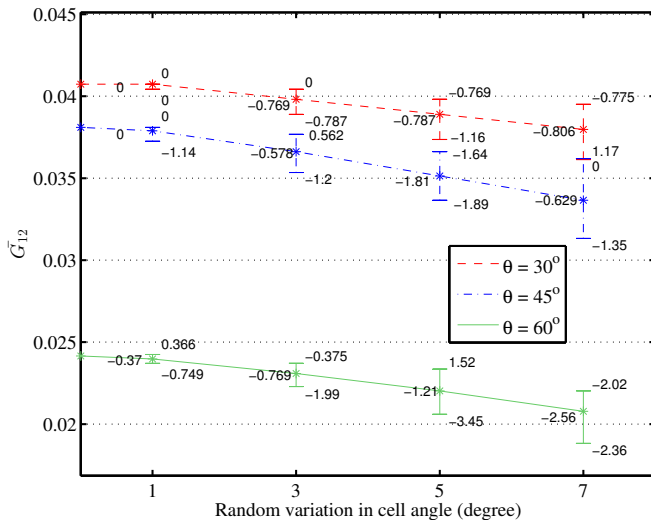


$$h/l = 1.5$$

# Poisson's ratio $\nu_{21}$

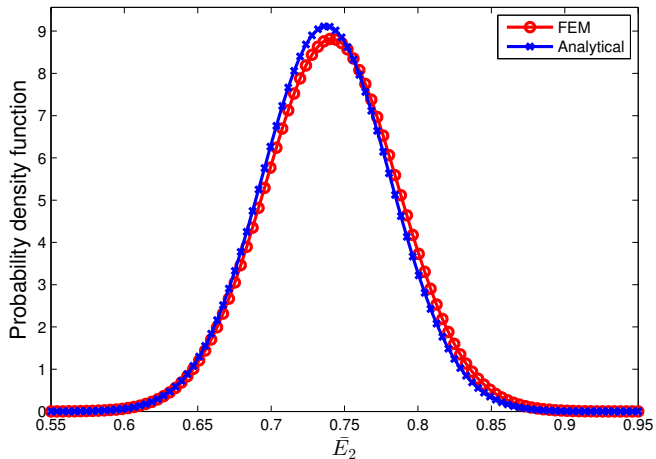


$h/l = 1.5$

Shear modulus ( $G_{12}$ )

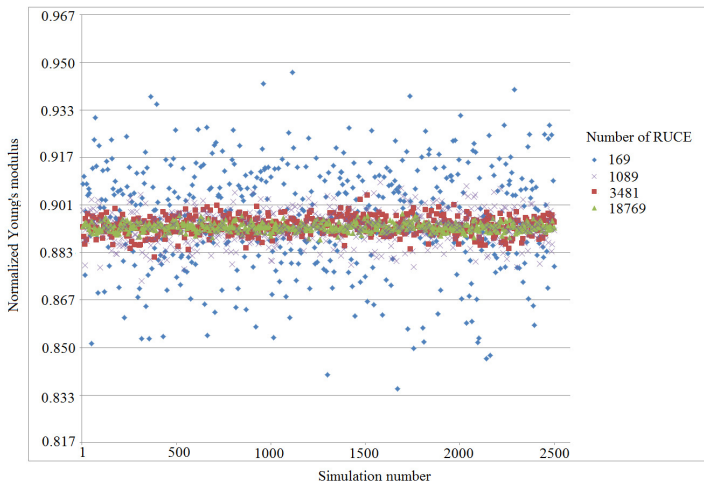
$$h/l = 1.5, \bar{G}_{12} = G_{12eq}/E_s\rho^3$$

# Probability density function of $E_2$



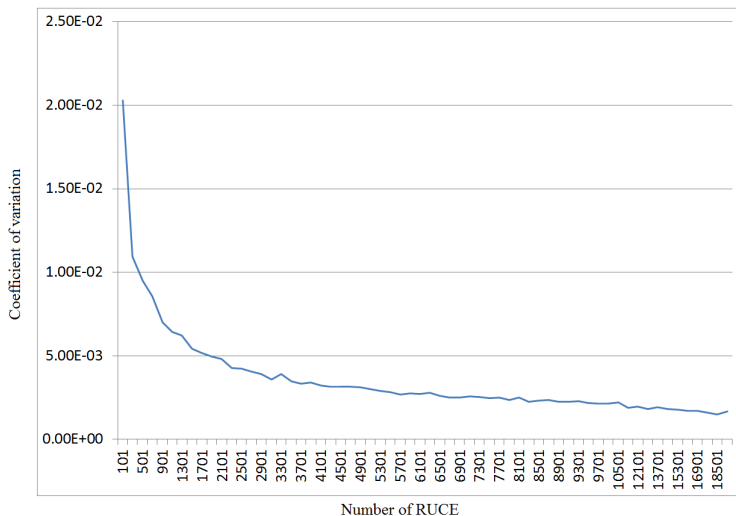
$$h/l = 1.5, \bar{E}_2 = E_{2eq}/E_{regular}, \theta = 45^\circ, \Delta\theta = 5^\circ$$

## Ergodic behaviour of $E_2$ : spread of values



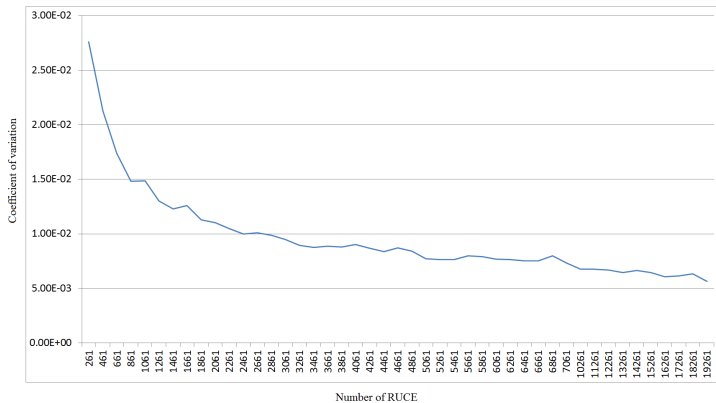
$$h/l = 1.5, \bar{E}_2 = E_{2eq}/E_{regular}, \theta = 45^\circ, \Delta\theta = 5^\circ$$

## Ergodic behaviour of $E_2$ : coefficient of variation



$$h/l = 1.5, \theta = 45^\circ, \Delta\theta = 5^\circ$$

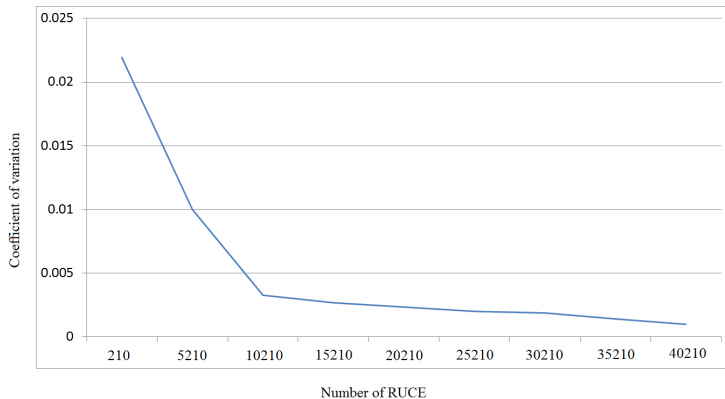
# Ergodic behaviour of $\nu_{21}$ : coefficient of variation



$$h/l = 1.5, \theta = 45^\circ, \Delta\theta = 5^\circ$$



## Ergodic behaviour of $G_{12}$ : coefficient of variation


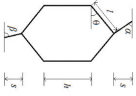



$$h/l = 1.5, \theta = 45^\circ, \Delta\theta = 5^\circ$$

## Main observations

- The elastic moduli obtained using the analytical method and by finite element simulation are in good agreement - establishing the validity of the closed-form expressions.
- The number of input random variables (cell angle) increase with the number of cells.
- The variation in  $E_1$  and  $\nu_{12}$  due to spatially random variations in cell angles is very less, while there is considerable amount of reductions in the values of  $E_2$ ,  $\nu_{21}$  and  $G_{12}$  with increasing degree of irregularity.
- Longitudinal Young's modulus, transverse Young's modulus and shear modulus are functions of both structural geometry and material properties of the irregular honeycomb (i.e. ratios  $h/l$ ,  $t/l$ ,  $s/l$  and angles  $\theta$ ,  $\alpha$ ,  $\beta$  and  $E_s$ ), while the Poisson's ratios depend only on structural geometry of irregular honeycombs (i.e. ratios  $h/l$ ,  $t/l$ ,  $s/l$  and angles  $\theta$ ,  $\alpha$ ,  $\beta$ )
- For large number of random cells ( $\approx 1700$ ), we observe the emergence of an effective ergodic behaviour - ensemble statistics become close to single sample "statistics".

# Conclusions

Irregular honeycomb	Representative unit cell element (RUCE)	Regular honeycomb	Parameter
			Structural configuration
$E_{1eq} = \frac{1}{\sum_{j=1}^n B_j} \sum_{j=1}^n \left( \frac{\sum_{i=1}^m l_{ij} \cos \theta_{ij}}{\sum_{i=1}^m B_{1U/ij}} \right) B_j$	$E_{1U} = E_s \left(\frac{t}{i}\right)^3 \frac{\cos \theta}{(\frac{h}{i} + \sin \theta) \sin^2 \theta}$	$E_{1GA} = E_s \left(\frac{t}{i}\right)^3 \frac{\cos \theta}{(\frac{h}{i} + \sin \theta) \sin^2 \theta}$	$E_1$
$E_{2eq} = \frac{1}{\left( \frac{\sum_{j=1}^n B_j \sum_{i=1}^m l_{ij} \cos \theta_{ij}}{\sum_{i=1}^m E_{2U/ij} l_{ij} \cos \theta_{ij}} \right)} \sum_{j=1}^n B_j$	$E_{2U} = E_s \left(\frac{t}{i}\right)^3 \frac{(\frac{h}{i} + 2\frac{t}{i} + 2 \sin \theta)}{\cos \theta (2 \cos^2 \theta + 8(\frac{t}{i})^3 (\frac{\cos^2 \alpha + \cos^2 \beta}{\sin^3 \alpha + \sin^3 \beta}) + 2(\frac{t}{i})^3 (\cot^2 \alpha + \cot^2 \beta))}$	$E_{2GA} = E_s \left(\frac{t}{i}\right)^3 \frac{(\frac{h}{i} + \sin \theta)}{\cos^3 \theta}$	$E_2$
$\nu_{12eq} = \frac{1}{\sum_{j=1}^n B_j} \sum_{j=1}^n \left( \frac{\sum_{i=1}^m l_{ij} \cos \theta_{ij}}{\sum_{i=1}^m \nu_{12U/ij}} \right) B_j$	$\nu_{12U} = \frac{2 \cos^2 \theta}{(2 \sin \theta + 2\frac{t}{i} + \frac{h}{i}) \sin \theta}$	$\nu_{12GA} = \frac{\cos^2 \theta}{(\frac{h}{i} + \sin \theta) \sin \theta}$	$\nu_{12}$
$\nu_{21eq} = \frac{1}{\left( \frac{\sum_{j=1}^n B_j \sum_{i=1}^m l_{ij} \cos \theta_{ij}}{\sum_{i=1}^m \nu_{21U/ij} l_{ij} \cos \theta_{ij}} \right)} \sum_{j=1}^n B_j$	$\nu_{21U} = \frac{\sin \theta (\frac{h}{i} + 2\frac{t}{i} + 2 \sin \theta)}{2 \cos^2 \theta + 8(\frac{t}{i})^3 (\frac{\cos^2 \alpha + \cos^2 \beta}{\sin^3 \alpha + \sin^3 \beta}) + 2(\frac{t}{i})^3 (\cot^2 \alpha + \cot^2 \beta)}$	$\nu_{21GA} = \frac{(\frac{h}{i} + \sin \theta) \sin \theta}{\cos^2 \theta}$	$\nu_{21}$
$G_{12eq} = \frac{1}{\left( \frac{\sum_{j=1}^n B_j \sum_{i=1}^m l_{ij} \cos \theta_{ij}}{\sum_{i=1}^m G_{12U/ij} l_{ij} \cos \theta_{ij}} \right)} \sum_{j=1}^n B_j$	$G_{12U} = E_s \left(\frac{t}{i}\right)^3 \frac{(2\frac{t}{i} + \frac{h}{i} + 2 \sin \theta)}{2 \cos \theta (2(\frac{t}{i})^2 + 4(\frac{t}{i})^2 (\frac{1}{\sin \alpha} + \frac{1}{\sin \beta}) + \frac{1}{2}(\frac{h}{i})^2 + (\frac{t}{i} + \sin \theta)(\frac{h}{i})^2)}$	$G_{12GA} = E_s \left(\frac{t}{i}\right)^3 \frac{(\frac{h}{i} + \sin \theta)}{(\frac{h}{i})^2 (1 + 2\frac{h}{i}) \cos \theta}$	$G_{12}$

In-plane elastic properties

## Some publications

- Mukhopadhyay, T. and Adhikari, S., “Free vibration of sandwich panels with randomly irregular honeycomb core”, [ASCE Journal of Engineering Mechanics](#), in press.
- Mukhopadhyay, T. and Adhikari, S., “Equivalent in-plane elastic properties of irregular honeycombs: An analytical approach”, [International Journal of Solids and Structures](#), 91[8] (2016), pp. 169-184.
- Mukhopadhyay, T. and Adhikari, S., “Effective in-plane elastic properties of auxetic honeycombs with spatial irregularity”, [Mechanics of Materials](#), 95[2] (2016), pp. 204-222.

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