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# Random Matrix Method for Stochastic Structural Mechanics

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# Stochastic structural dynamics

- The equation of motion:

$$\mathbf{M}\ddot{\mathbf{x}}(t) + \mathbf{C}\dot{\mathbf{x}}(t) + \mathbf{K}\mathbf{x}(t) = \mathbf{p}(t)$$

- Due to the presence of uncertainty  $\mathbf{M}$ ,  $\mathbf{C}$  and  $\mathbf{K}$  become random matrices.
- The main objectives are:
  - to quantify uncertainties in the system matrices
  - to predict the variability in the response vector  $\mathbf{x}$

# Current Methods

Two different approaches are currently available

- **Low frequency** : **Stochastic Finite Element Method (SFEM)** - considers parametric uncertainties in details
- **High frequency** : **Statistical Energy Analysis (SEA)** - do not consider parametric uncertainties in details

**Work needs to be done** : **Medium frequency vibration problems** - some kind of 'combination' of the above two

# Random Matrix Method (RMM)

- **The objective**: To have an **unified method** which will work across the frequency range.
- **The methodology**:
  - Derive the matrix variate probability density functions of  $M$ ,  $C$  and  $K$
  - Propagate the uncertainty (using Monte Carlo simulation or analytical methods) to obtain the response statistics (or pdf)

# Outline of the presentation

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In what follows next, I will discuss:

- Introduction to Matrix variate distributions
- Maximum entropy distribution
- Optimal Wishart distribution
- Numerical examples
- Open problems & discussions

# Matrix variate distributions

- The probability density function of a random matrix can be defined in a manner similar to that of a random variable.
- If  $\mathbf{A}$  is an  $n \times m$  real random matrix, the matrix variate probability density function of  $\mathbf{A} \in \mathbb{R}_{n,m}$ , denoted as  $p_{\mathbf{A}}(\mathbf{A})$ , is a mapping from the space of  $n \times m$  real matrices to the real line, i.e.,  $p_{\mathbf{A}}(\mathbf{A}) : \mathbb{R}_{n,m} \rightarrow \mathbb{R}$ .

# Gaussian random matrix

The random matrix  $\mathbf{X} \in \mathbb{R}_{n,p}$  is said to have a matrix variate Gaussian distribution with mean matrix  $\mathbf{M} \in \mathbb{R}_{n,p}$  and covariance matrix  $\Sigma \otimes \Psi$ , where  $\Sigma \in \mathbb{R}_n^+$  and  $\Psi \in \mathbb{R}_p^+$  provided the pdf of  $\mathbf{X}$  is given by

$$p_{\mathbf{X}}(\mathbf{X}) = (2\pi)^{-np/2} |\Sigma|^{-p/2} |\Psi|^{-n/2} \operatorname{etr} \left\{ -\frac{1}{2} \Sigma^{-1} (\mathbf{X} - \mathbf{M}) \Psi^{-1} (\mathbf{X} - \mathbf{M})^T \right\} \quad (1)$$

This distribution is usually denoted as  $\mathbf{X} \sim N_{n,p}(\mathbf{M}, \Sigma \otimes \Psi)$ .

# Wishart matrix

A  $n \times n$  symmetric positive definite random matrix  $\mathbf{S}$  is said to have a Wishart distribution with parameters  $p \geq n$  and  $\Sigma \in \mathbb{R}_n^+$ , if its pdf is given by

$$p_{\mathbf{S}}(\mathbf{S}) = \left\{ 2^{\frac{1}{2}np} \Gamma_n \left( \frac{1}{2}p \right) |\Sigma|^{\frac{1}{2}p} \right\}^{-1} |\mathbf{S}|^{\frac{1}{2}(p-n-1)} \text{etr} \left\{ -\frac{1}{2} \Sigma^{-1} \mathbf{S} \right\} \quad (2)$$

This distribution is usually denoted as  $\mathbf{S} \sim W_n(p, \Sigma)$ .

**Note:** If  $p = n + 1$ , then the matrix is non-negative definite.



# Matrix variate Gamma distribution

A  $n \times n$  symmetric positive definite matrix random  $\mathbf{W}$  is said to have a matrix variate gamma distribution with parameters  $a$  and  $\Psi \in \mathbb{R}_n^+$ , if its pdf is given by

$$p_{\mathbf{W}}(\mathbf{W}) = \left\{ \Gamma_n(a) |\Psi|^{-a} \right\}^{-1} |\mathbf{W}|^{a - \frac{1}{2}(n+1)} \text{etr} \{ -\Psi \mathbf{W} \}; \quad \Re(a) > \frac{1}{2}(n-1) \quad (3)$$

This distribution is usually denoted as  $\mathbf{W} \sim G_n(a, \Psi)$ . Here the multivariate gamma function:

$$\Gamma_n(a) = \pi^{\frac{1}{4}n(n-1)} \prod_{k=1}^n \Gamma \left[ a - \frac{1}{2}(k-1) \right]; \quad \text{for } \Re(a) > (n-1)/2 \quad (4)$$

# Inverted Wishart matrix

A  $n \times n$  symmetric positive definite matrix random  $\mathbf{V}$  is said to have an inverted Wishart distribution with parameters  $m$  and  $\Psi \in \mathbb{R}_n^+$ , if its pdf is given by

$$p_{\mathbf{V}}(\mathbf{V}) = \frac{2^{-\frac{1}{2}(m-n-1)n} |\Psi|^{\frac{1}{2}(m-n-1)}}{\Gamma_n\left(\frac{1}{2}(m-n-1)\right) |\mathbf{V}|^{m/2}} \text{etr}\{-\mathbf{V}^{-1}\Psi\}; \quad m > 2n, \Psi > 0. \quad (5)$$

This distribution is usually denoted as  $\mathbf{V} \sim IW_n(m, \Psi)$ .

# Distribution of the system matrices

The distribution of the random system matrices  $\mathbf{M}$ ,  $\mathbf{C}$  and  $\mathbf{K}$  should be such that they are

- symmetric
- positive-definite, and
- the moments (at least first two) of the inverse of the dynamic stiffness matrix

$$\mathbf{D}(\omega) = -\omega^2\mathbf{M} + i\omega\mathbf{C} + \mathbf{K} \text{ should exist } \forall \omega$$

# Distribution of the system matrices

- The exact application of the last constraint requires the derivation of the joint probability density function of  $\mathbf{M}$ ,  $\mathbf{C}$  and  $\mathbf{K}$ , which is quite difficult to obtain.
- We consider a simpler problem where it is required that the inverse moments of each of the system matrices  $\mathbf{M}$ ,  $\mathbf{C}$  and  $\mathbf{K}$  must exist.
- Provided the system is damped, this will guarantee the existence of the moments of the frequency response function matrix.

# Maximum Entropy Distribution

Suppose that the mean values of  $\mathbf{M}$ ,  $\mathbf{C}$  and  $\mathbf{K}$  are given by  $\overline{\mathbf{M}}$ ,  $\overline{\mathbf{C}}$  and  $\overline{\mathbf{K}}$  respectively. Using the notation  $\mathbf{G}$  (which stands for any one the system matrices) the matrix variate density function of  $\mathbf{G} \in \mathbb{R}_n^+$  is given by  $p_{\mathbf{G}}(\mathbf{G}) : \mathbb{R}_n^+ \rightarrow \mathbb{R}$ . We have the following constraints to obtain  $p_{\mathbf{G}}(\mathbf{G})$ :

$$\int_{\mathbf{G}>0} p_{\mathbf{G}}(\mathbf{G}) d\mathbf{G} = 1 \quad (\text{normalization}) \quad (6)$$

and 
$$\int_{\mathbf{G}>0} \mathbf{G} p_{\mathbf{G}}(\mathbf{G}) d\mathbf{G} = \overline{\mathbf{G}} \quad (\text{the mean matrix})$$

(7)

# Further constraints

- Suppose the inverse moments (say up to order  $\nu$ ) of the system matrix exist. This implies that  $E [\|\mathbf{G}^{-1}\|_F^\nu]$  should be finite. Here the Frobenius norm of matrix  $\mathbf{A}$  is given by
$$\|\mathbf{A}\|_F = (\text{Trace}(\mathbf{A}\mathbf{A}^T))^{1/2}.$$
- Taking the logarithm for convenience, the condition for the existence of the inverse moments can be expressed by

$$E [\ln |\mathbf{G}|^{-\nu}] < \infty$$

# MEnt Distribution - 1

The Lagrangian becomes:

$$\begin{aligned} \mathcal{L}(p_{\mathbf{G}}) = & - \int_{\mathbf{G}>0} p_{\mathbf{G}}(\mathbf{G}) \ln \{p_{\mathbf{G}}(\mathbf{G})\} d\mathbf{G} - \\ & (\lambda_0 - 1) \left( \int_{\mathbf{G}>0} p_{\mathbf{G}}(\mathbf{G}) d\mathbf{G} - 1 \right) - \nu \int_{\mathbf{G}>0} \ln |\mathbf{G}| p_{\mathbf{G}} d\mathbf{G} \\ & + \text{Trace} \left( \Lambda_1 \left[ \int_{\mathbf{G}>0} \mathbf{G} p_{\mathbf{G}}(\mathbf{G}) d\mathbf{G} - \overline{\mathbf{G}} \right] \right) \quad (8) \end{aligned}$$

Note:  $\nu$  cannot be obtained uniquely!

# MEnt Distribution - 2

Using the calculus of variation

$$\frac{\partial \mathcal{L}(p_{\mathbf{G}})}{\partial p_{\mathbf{G}}} = 0$$

or  $-\ln \{p_{\mathbf{G}}(\mathbf{G})\} = \lambda_0 + \text{Trace}(\Lambda_1 \mathbf{G}) - \ln |\mathbf{G}|^\nu$

or  $p_{\mathbf{G}}(\mathbf{G}) = \exp\{-\lambda_0\} |\mathbf{G}|^\nu \text{etr}\{-\Lambda_1 \mathbf{G}\}$



# MEnt Distribution - 3

Using the matrix variate Laplace transform  
( $\mathbf{T} \in \mathbb{R}_{n,n}$ ,  $\mathbf{S} \in \mathbb{C}_{n,n}$ ,  $a > (n + 1)/2$ )

$$\int_{\mathbf{T} > 0} \text{etr} \{ -\mathbf{S}\mathbf{T} \} |\mathbf{T}|^{a-(n+1)/2} d\mathbf{T} = \Gamma_n(a) |\mathbf{S}|^{-a}$$

and substituting  $p_{\mathbf{G}}(\mathbf{G})$  into the constraint equations it can be shown that

$$p_{\mathbf{G}}(\mathbf{G}) = \frac{r^{nr} |\overline{\mathbf{G}}|^{-r}}{\Gamma_n(r)} |\mathbf{G}|^\nu \text{etr} \left\{ -r \overline{\mathbf{G}}^{-1} \mathbf{G} \right\} \quad (9)$$

where  $r = \nu + (n + 1)/2$ .

# MEnt Distribution - 4

Comparing it with the Wishart distribution we have:

**Theorem 1.** *If  $\nu$ -th order inverse-moment of a system matrix  $\mathbf{G} \equiv \{\mathbf{M}, \mathbf{C}, \mathbf{K}\}$  exists and only the mean of  $\mathbf{G}$  is available, say  $\overline{\mathbf{G}}$ , then the maximum-entropy pdf of  $\mathbf{G}$  follows the Wishart distribution with parameters  $p = (2\nu + n + 1)$  and  $\Sigma = \overline{\mathbf{G}} / (2\nu + n + 1)$ , that is*

$$\mathbf{G} \sim W_n(2\nu + n + 1, \overline{\mathbf{G}} / (2\nu + n + 1)).$$

# Properties of the Distribution

- Covariance tensor of  $\mathbf{G}$ :

$$\text{cov} (G_{ij}, G_{kl}) = \frac{1}{2\nu + n + 1} (\overline{G}_{ik}\overline{G}_{jl} + \overline{G}_{il}\overline{G}_{jk})$$

- Normalized standard deviation matrix

$$\delta_{\mathbf{G}}^2 = \frac{\mathbb{E} [\|\mathbf{G} - \mathbb{E}[\mathbf{G}]\|_{\text{F}}^2]}{\|\mathbb{E}[\mathbf{G}]\|_{\text{F}}^2} = \frac{1}{2\nu + n + 1} \left\{ 1 + \frac{\{\text{Trace}(\overline{\mathbf{G}})\}^2}{\text{Trace}(\overline{\mathbf{G}}^2)} \right\}$$

- $\delta_{\mathbf{G}}^2 \leq \frac{1+n}{2\nu+n+1}$  and  $\nu \uparrow \Rightarrow \delta_{\mathbf{G}}^2 \downarrow$ .

# Distribution of the inverse - 1

- If  $\mathbf{G}$  is  $W_n(p, \Sigma)$  then  $\mathbf{V} = \mathbf{G}^{-1}$  has the inverted Wishart distribution:

$$P_{\mathbf{V}}(\mathbf{V}) = \frac{2^{m-n-1} n/2 |\Psi|^{m-n-1} /2}{\Gamma_n[(m-n-1)/2] |\mathbf{V}|^{m/2}} \text{etr} \left\{ -\frac{1}{2} \mathbf{V}^{-1} \Psi \right\}$$

where  $m = n + p + 1$  and  $\Psi = \Sigma^{-1}$  (recall that  $p = 2\nu + n + 1$  and  $\Sigma = \overline{\mathbf{G}}/p$ )

# Distribution of the inverse - 2

- Mean:  $E[G^{-1}] = \frac{p\bar{G}^{-1}}{p - n - 1}$
- $\text{cov}(G_{ij}^{-1}, G_{kl}^{-1}) =$   
$$\frac{(2\nu + n + 1)(\nu^{-1}\bar{G}_{ij}^{-1}\bar{G}_{kl}^{-1} + \bar{G}_{ik}^{-1}\bar{G}_{jl}^{-1} + \bar{G}^{-1}il\bar{G}_{kj}^{-1})}{2\nu(2\nu + 1)(2\nu - 2)}$$

# Distribution of the inverse - 3

- Suppose  $n = 101$  &  $\nu = 2$ . So  $p = 2\nu + n + 1 = 106$  and  $p - n - 1 = 4$ . Therefore,  $E[\mathbf{G}] = \overline{\mathbf{G}}$  and  $E[\mathbf{G}^{-1}] = \frac{106}{4}\overline{\mathbf{G}}^{-1} = 26.5\overline{\mathbf{G}}^{-1}$  !!!!!!!!!!!!!
- From a practical point of view we do not expect them to be so far apart!
- One way to reduce the gap is to increase  $p$ . But this implies the reduction of variance.
- This discrepancy between the ‘mean of the inverse’ and the ‘inverse of the mean’ of the random matrices appears to be a fundamental limitation.

# Optimal Wishart Distribution - 1

- **My argument:** The distribution of  $\mathbf{G}$  must be such that  $E[\mathbf{G}]$  and  $E[\mathbf{G}^{-1}]$  should be closest to  $\overline{\mathbf{G}}$  and  $\overline{\mathbf{G}}^{-1}$  respectively.
- Suppose  $\mathbf{G} \sim W_n(n + 1 + \theta, \overline{\mathbf{G}}/\alpha)$ . We need to find  $\alpha$  such that the above condition is satisfied.
- Therefore, define (and subsequently minimize)

**‘normalized errors’:**

$$\varepsilon_1 = \left\| \overline{\mathbf{G}} - E[\mathbf{G}] \right\|_{\text{F}} / \left\| \overline{\mathbf{G}} \right\|_{\text{F}}$$

$$\varepsilon_2 = \left\| \overline{\mathbf{G}}^{-1} - E[\mathbf{G}^{-1}] \right\|_{\text{F}} / \left\| \overline{\mathbf{G}}^{-1} \right\|_{\text{F}}$$

# Optimal Wishart Distribution - 2

Because  $\mathbf{G} \sim W_n(n + 1 + \theta, \bar{\mathbf{G}}/\alpha)$  we have

$$\mathbb{E}[\mathbf{G}] = \frac{n + 1 + \theta}{\alpha} \bar{\mathbf{G}}$$

$$\text{and } \mathbb{E}[\mathbf{G}^{-1}] = \frac{\alpha}{\theta} \bar{\mathbf{G}}^{-1}$$

We define the objective function to be minimized as

$$\chi^2 = \varepsilon_1^2 + \varepsilon_2^2 = \left(1 - \frac{n+1+\theta}{\alpha}\right)^2 + \left(1 - \frac{\alpha}{\theta}\right)^2$$



# Optimal Wishart Distribution - 3

The optimal value of  $\alpha$  can be obtained as by

setting  $\frac{\partial \chi^2}{\partial \alpha} = 0$  or

$$\alpha^4 - \alpha^3 \theta - \theta^4 + (-2n + \alpha - 2) \theta^3 + ((n + 1) \alpha - n^2 - 2n - 1) \theta^2 = 0.$$

The only feasible value of  $\alpha$  is

$$\alpha = \sqrt{\theta(n + 1 + \theta)}$$

# Optimal Wishart Distribution - 4

From this discussion we have the following:

**Theorem 2.** *If  $\nu$ -th order inverse-moment of a system matrix  $\mathbf{G} \equiv \{\mathbf{M}, \mathbf{C}, \mathbf{K}\}$  exists and only the mean of  $\mathbf{G}$  is available, say  $\overline{\mathbf{G}}$ , then the unbiased distribution of  $\mathbf{G}$  follows the Wishart distribution with parameters  $p = (2\nu + n + 1)$  and*

$\Sigma = \overline{\mathbf{G}} / \sqrt{2\nu(2\nu + n + 1)}$ , that is

$\mathbf{G} \sim W_n \left( 2\nu + n + 1, \overline{\mathbf{G}} / \sqrt{2\nu(2\nu + n + 1)} \right)$ .

# Optimal Wishart Distribution - 5

- Again consider  $n = 100$  and  $\nu = 2$ , so that  $\theta = 2\nu = 4$ .
- In the previous approach  $\alpha = 2\nu + n + 1 = 105$ . For the optimal distribution,  $\alpha = \sqrt{\theta(\theta + n + 1)} = 2\sqrt{105} = 20.49$ .
- We have  $E[\mathbf{G}] = \frac{105}{2\sqrt{105}}\overline{\mathbf{G}} = 5.12\overline{\mathbf{G}}$  and  $E[\mathbf{G}^{-1}] = \frac{2\sqrt{105}}{4}\overline{\mathbf{G}}^{-1} = 5.12\overline{\mathbf{G}}^{-1}$ .
- The overall normalized difference for the previous case is  $\chi^2 = 0 + (1 - 105/4)^2 = 637.56$ . The same for the optimal distribution is  $\chi^2 = 2(1 - \sqrt{105}/2)^2 = 34.01$ , which is considerable smaller compared to the non-optimal distribution.

# Response statistics - 1

- The equation of motion is  $\mathbf{D}\mathbf{x} = \mathbf{p}$ ,  $\mathbf{D}$  is in general  $n \times n$  complex random matrix.
- The response is given by

$$\mathbf{x} = \mathbf{D}^{-1}\mathbf{p}$$

- Consider **static** problems so that all matrices/vectors are real.

# Response statistics - 2

- We may want statistics of few elements or some linear combinations of the elements in  $\mathbf{x}$ . So the quantify of interest is

$$\mathbf{y} = \mathbf{R}\mathbf{x} = \mathbf{R}\mathbf{D}^{-1}\mathbf{p} \quad (10)$$

Here  $\mathbf{R}$  is in general  $r \times n$  rectangular matrix. For the special case when  $\mathbf{R} = \mathbf{I}_n$ , we have  $\mathbf{y} = \mathbf{x}$ .

- Eq. (10) arises in SFEM. There are many papers on its solution. Mainly perturbation methods are used.

# Response statistics - 3

Suppose  $\mathbf{D} = \mathbf{D}_0 + \Delta\mathbf{D}$ , where  $\mathbf{D}_0$  is the deterministic part and  $\Delta\mathbf{D}$  is the (small) random part. It can be shown that

$$\mathbf{D}^{-1} = \mathbf{D}_0^{-1} - \mathbf{D}_0^{-1} \Delta\mathbf{D} \mathbf{D}_0^{-1} + \mathbf{D}_0^{-1} \Delta\mathbf{D} \mathbf{D}_0^{-1} \Delta\mathbf{D} \mathbf{D}_0^{-1} - \dots$$

From, this

$$\mathbf{y} = \mathbf{y}_0 - \mathbf{R} \mathbf{D}_0^{-1} \Delta\mathbf{D} \mathbf{x}_0 + \mathbf{R} \mathbf{D}_0^{-1} \Delta\mathbf{D} \mathbf{D}_0^{-1} \Delta\mathbf{D} \mathbf{x}_0 - \dots \quad (11)$$

where  $\mathbf{x}_0 = \mathbf{D}_0^{-1} \mathbf{p}$  and  $\mathbf{y}_0 = \mathbf{R} \mathbf{x}_0$ .

# Response statistics - 4

The statistics of  $y$  can be calculated from Eq. (11). However,

- The calculation is difficult if  $\Delta D$  is non-Gaussian.
- Even if  $\Delta D$  is Gaussian, inclusion of higher-order terms results very messy calculations (I have not seen any published work for more than second-order)
- For these reasons, the response statistics will be inaccurate for large randomness.

# Response statistics - 5

I will propose an **exact** method using RMT. Suppose  $\mathbf{D} \sim W_n(m, \Sigma)$ .

$$\mathbb{E}[\mathbf{y}] = \mathbb{E}[\mathbf{R}\mathbf{D}^{-1}\mathbf{p}] = \mathbf{R}\mathbb{E}[\mathbf{D}^{-1}]\mathbf{p} = \mathbf{R}\Sigma^{-1}\mathbf{p}/\theta \quad (12)$$

The complete covariance matrix of  $\mathbf{y}$

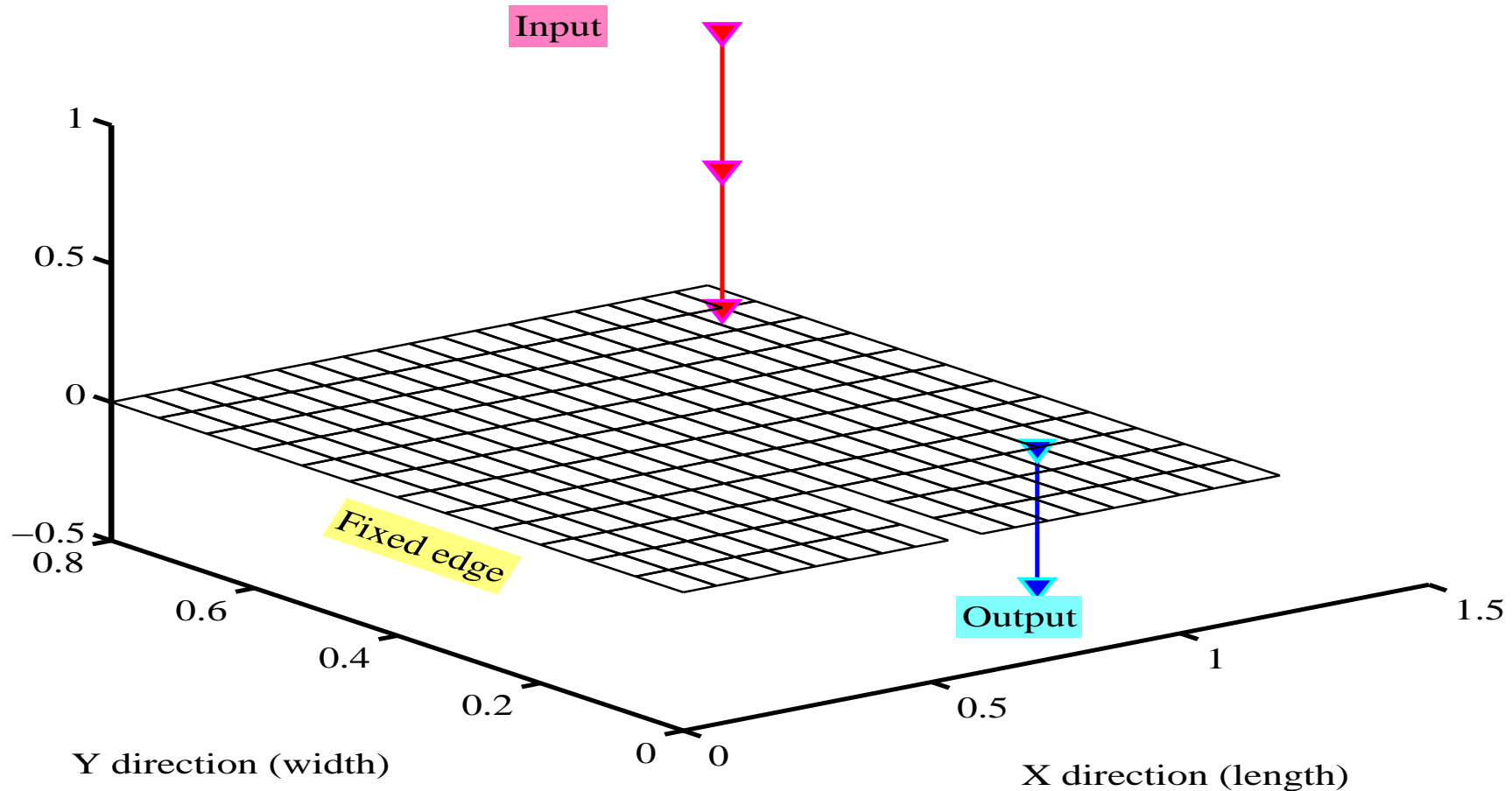
$$\begin{aligned} & \mathbb{E}[(\mathbf{y} - \mathbb{E}[\mathbf{y}])(\mathbf{y} - \mathbb{E}[\mathbf{y}])^T] \\ &= \mathbf{R}\mathbb{E}[\mathbf{D}^{-1}\mathbf{p}\mathbf{p}^T\mathbf{D}^{-1}]\mathbf{R}^T - \mathbb{E}[\mathbf{y}](\mathbb{E}[\mathbf{y}])^T \\ &= \frac{\text{Trace}(\Sigma^{-1}\mathbf{p}\mathbf{p}^T)\mathbf{R}\Sigma^{-1}\mathbf{R}^T}{\theta(\theta+1)(\theta-2)} + \frac{(\theta+2)\mathbf{R}\Sigma^{-1}\mathbf{p}\mathbf{p}^T\Sigma^{-1}\mathbf{R}^T}{\theta^2(\theta+1)(\theta-2)} \end{aligned} \quad (13)$$



# Simulation Algorithm: Dynamical Systems

- Obtain  $\theta = \frac{1}{\delta_{\mathbf{G}}^2} \left\{ 1 + \frac{\{\text{Trace}(\overline{\mathbf{G}})\}^2}{\text{Trace}(\overline{\mathbf{G}}^2)} \right\} - (n + 1)$
- If  $\theta < 4$ , then select  $\theta = 4$ .
- Calculate  $\alpha = \sqrt{\theta(n + 1 + \theta)}$
- Generate samples of  $\mathbf{G} \sim W_n(n + 1 + \theta, \overline{\mathbf{G}}/\alpha)$   
(MATLAB<sup>®</sup> command `wishrnd` can be used to generate the samples)
- Repeat the above steps for all system matrices and solve for every samples

# Example: A cantilever Plate

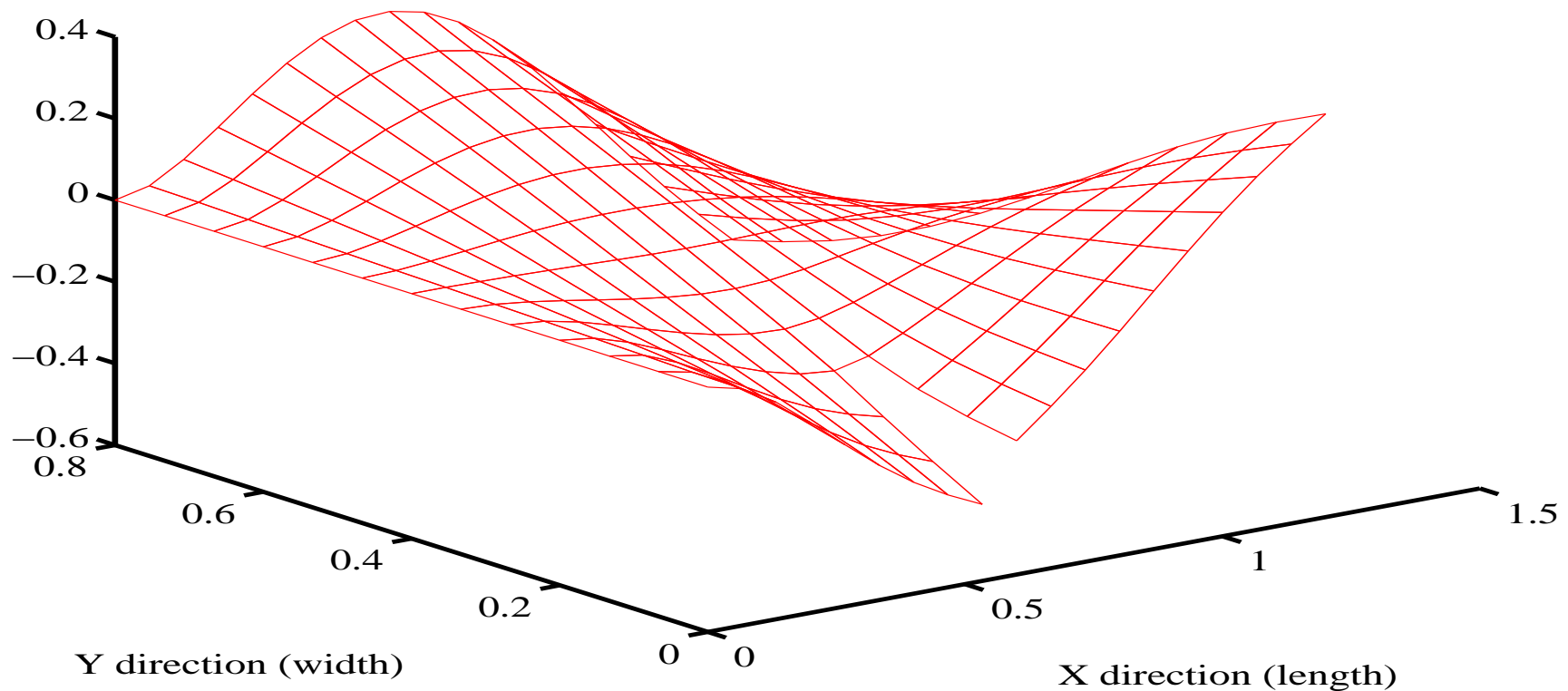


A Cantilever plate with a slot:  $\bar{E} = 200 \times 10^9 \text{N/m}^2$ ,  $\bar{\mu} = 0.3$ ,  $\bar{\rho} = 7860 \text{kg/m}^3$ ,  $\bar{t} = 7.5 \text{mm}$ ,

$$L_x = 1.2 \text{m}, L_y = 0.8 \text{m}.$$

# Plate Mode 4

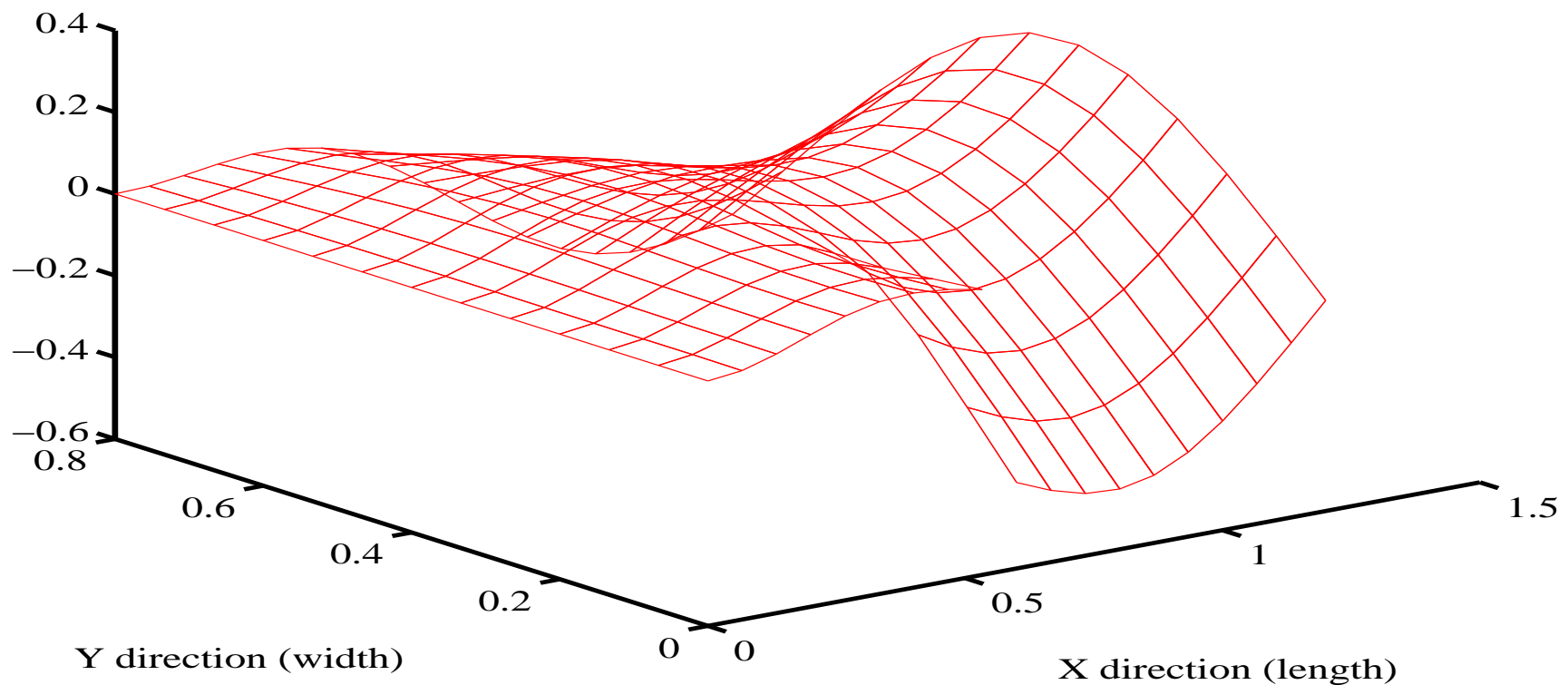
Mode 4, freq. = 48.745 Hz



## Fourth Mode shape

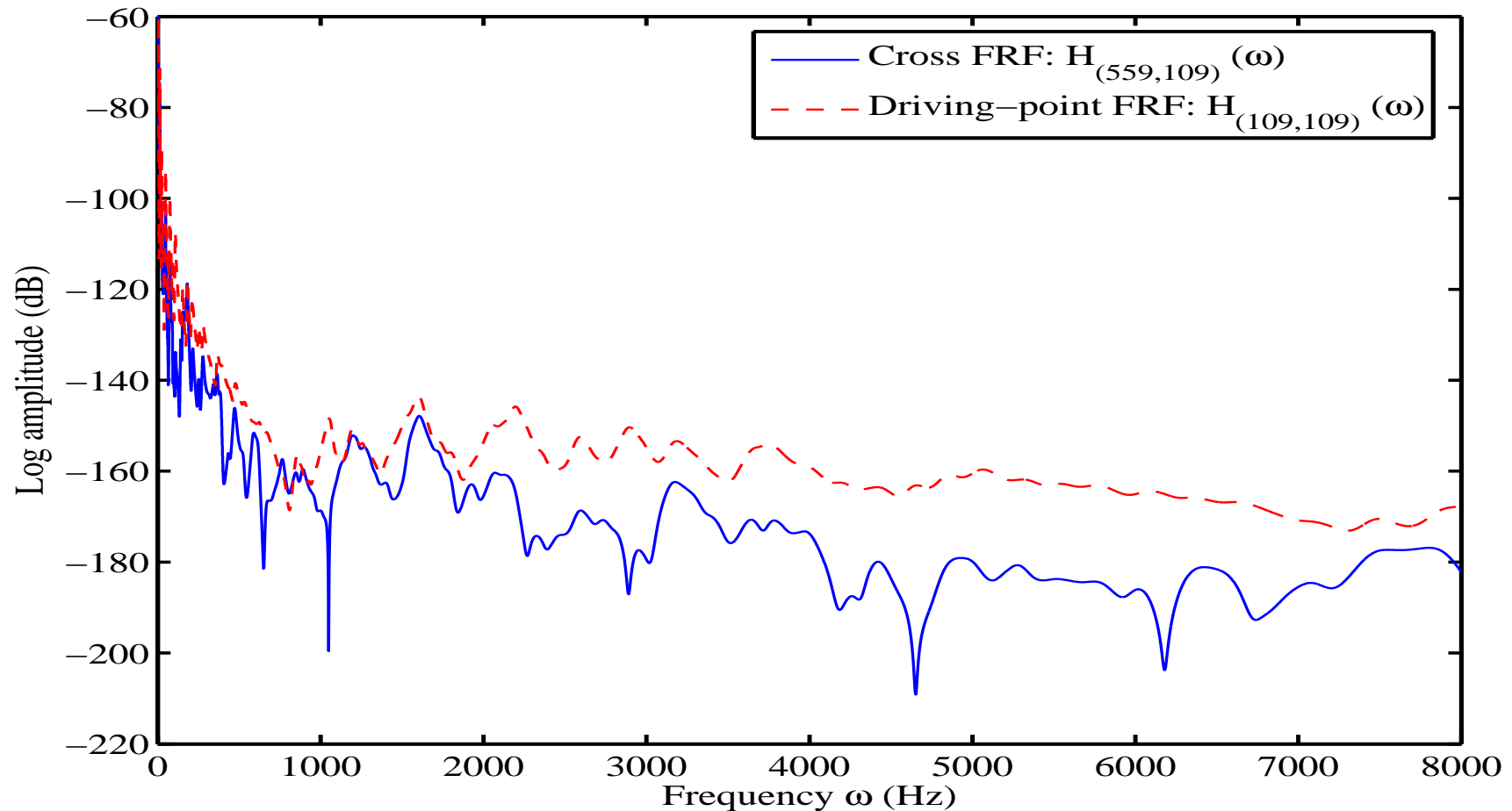
# Plate Mode 5

Mode 5, freq. = 64.3556 Hz



## Fifth Mode shape

# Deterministic FRF



FRF of the deterministic plate

# Stochastic Properties

The Young's modulus, Poissons ratio, mass density and thickness are random fields of the form

$$E(\mathbf{x}) = \bar{E} (1 + \epsilon_E f_1(\mathbf{x})) \quad (14)$$

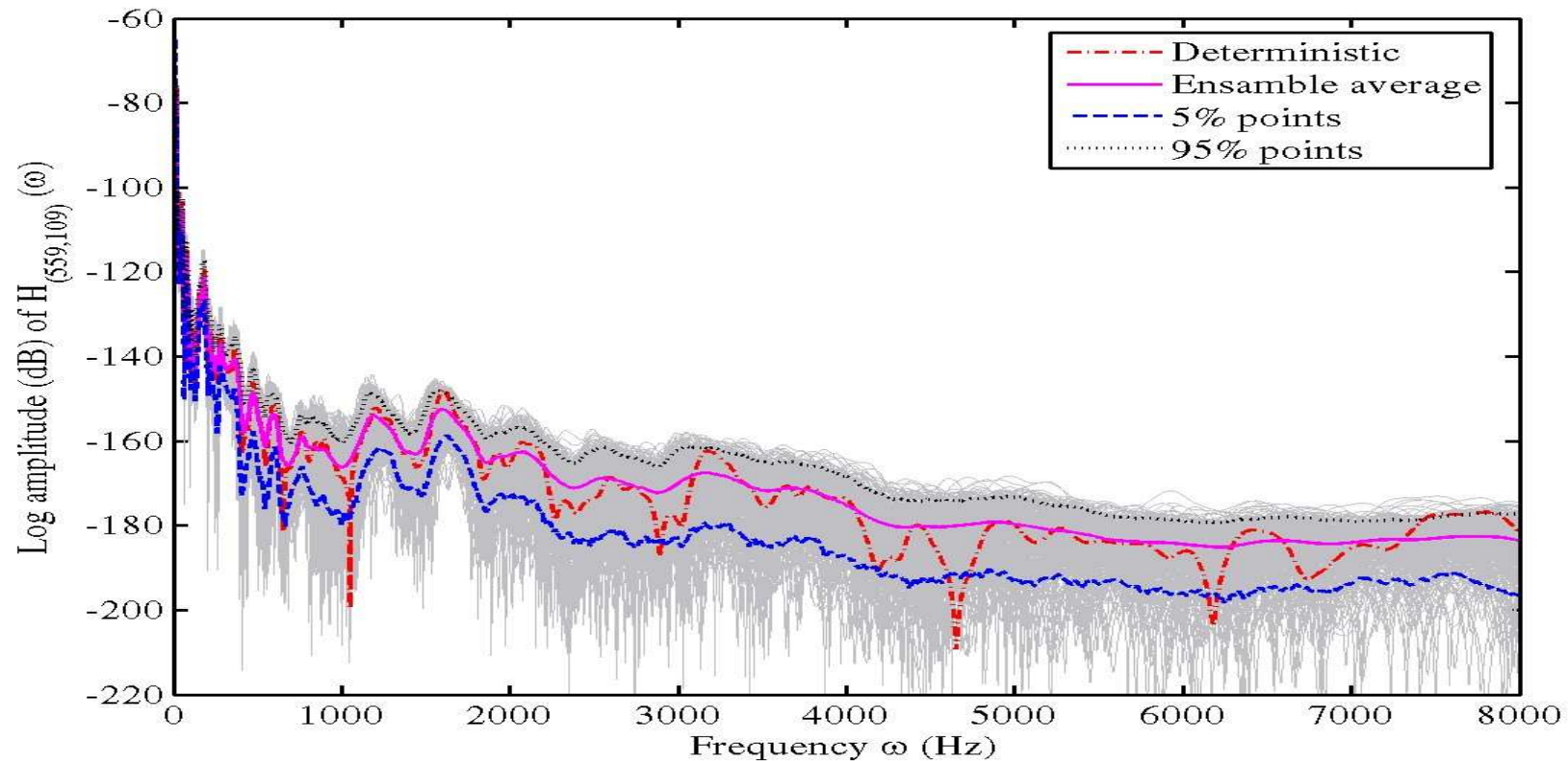
$$\mu(\mathbf{x}) = \bar{\mu} (1 + \epsilon_\mu f_2(\mathbf{x})) \quad (15)$$

$$\rho(\mathbf{x}) = \bar{\rho} (1 + \epsilon_\rho f_3(\mathbf{x})) \quad (16)$$

$$\text{and } t(\mathbf{x}) = \bar{t} (1 + \epsilon_t f_4(\mathbf{x})) \quad (17)$$

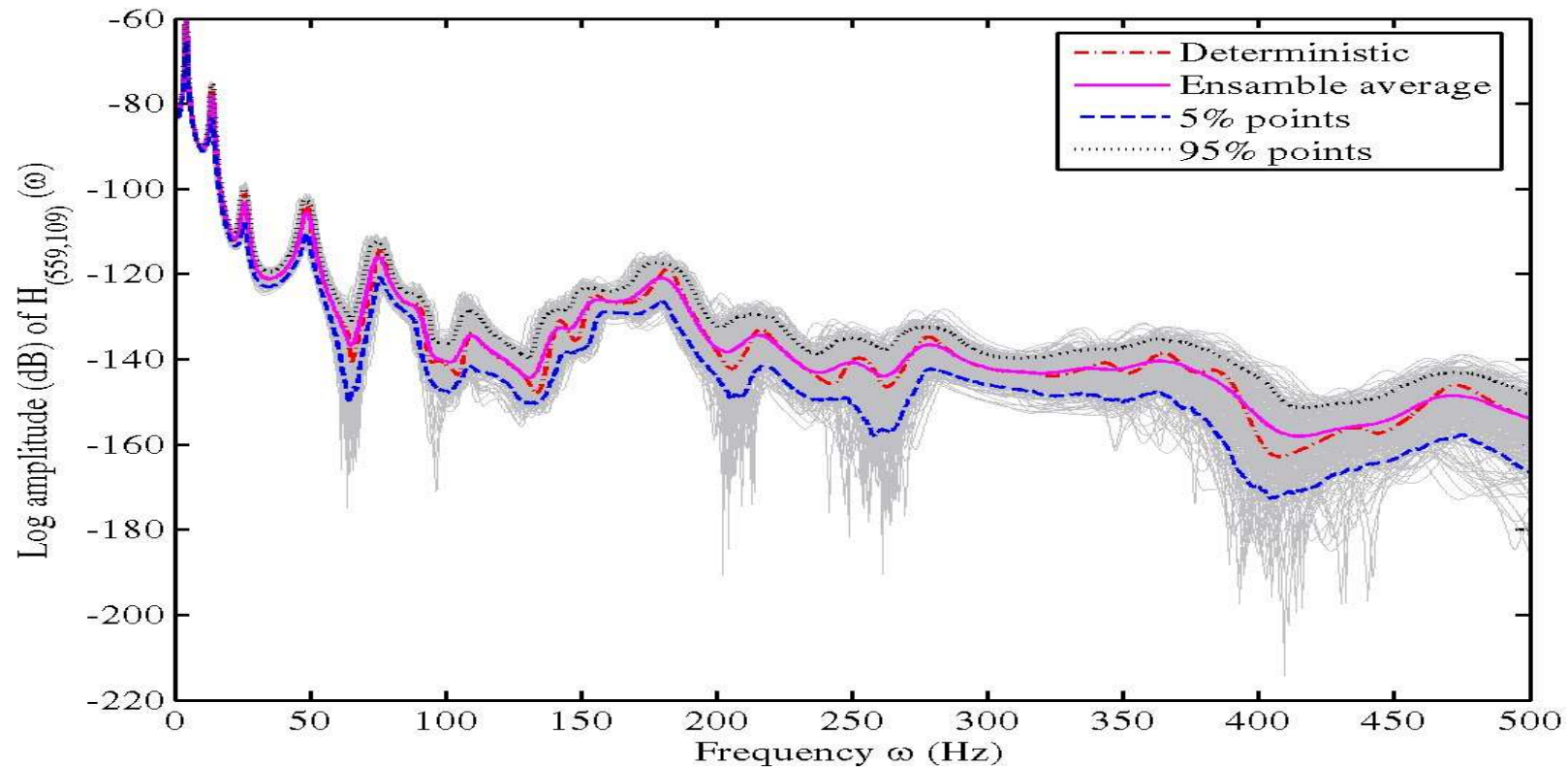
- The strength parameters:  $\epsilon_E = 0.15$ ,  $\epsilon_\mu = 0.15$ ,  $\epsilon_\rho = 0.10$  and  $\epsilon_t = 0.15$ .
- The random fields  $f_i(\mathbf{x})$ ,  $i = 1, \dots, 4$  are delta-correlated homogenous Gaussian random fields.

# SFEM cross-FRF



Direct stochastic finite-element Monte Carlo Simulation of the amplitude of the cross-FRF.

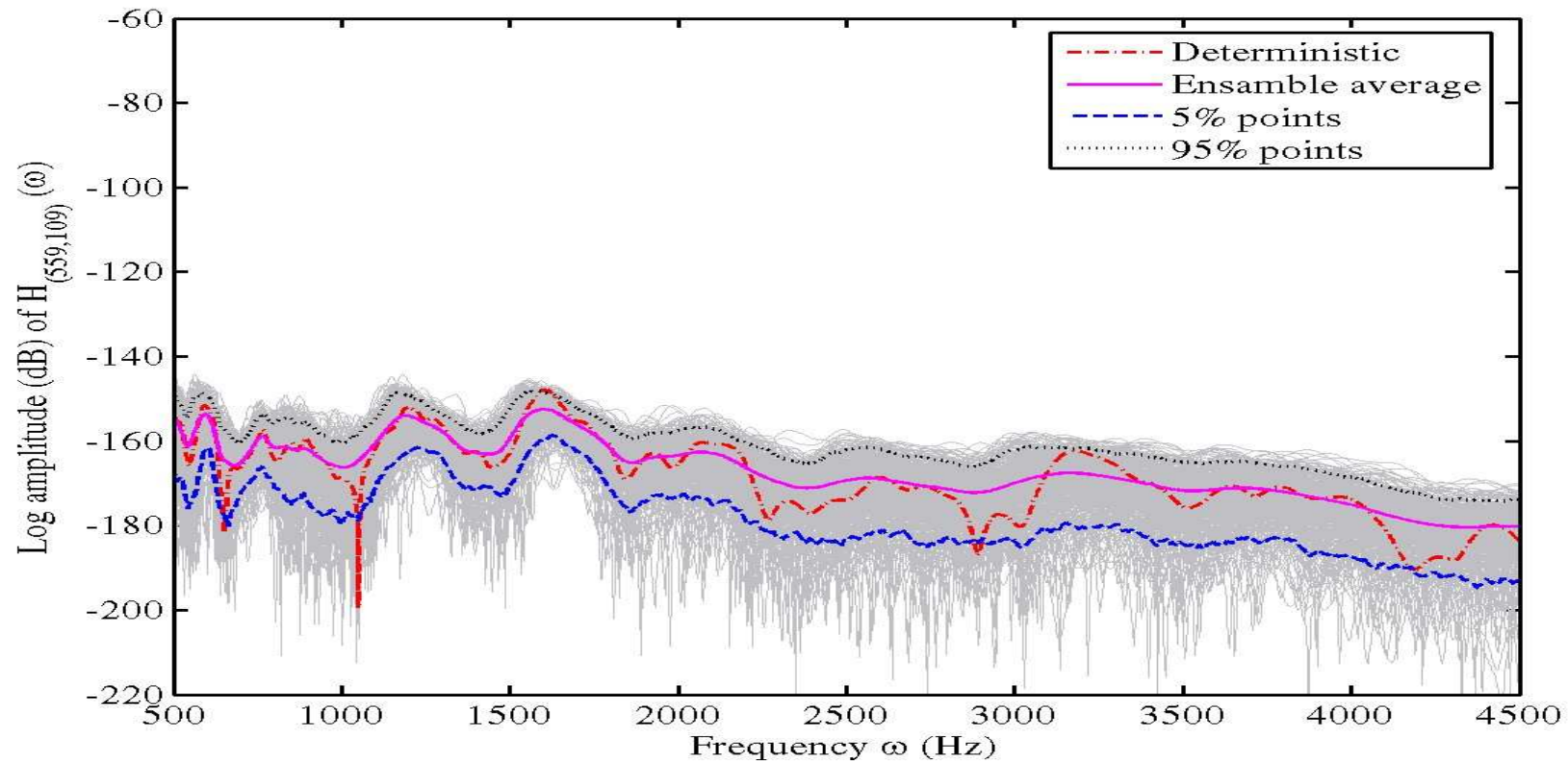
# SFEM cross-FRF: Low Freq



Direct stochastic finite-element Monte Carlo Simulation of the amplitude of the cross-FRF.

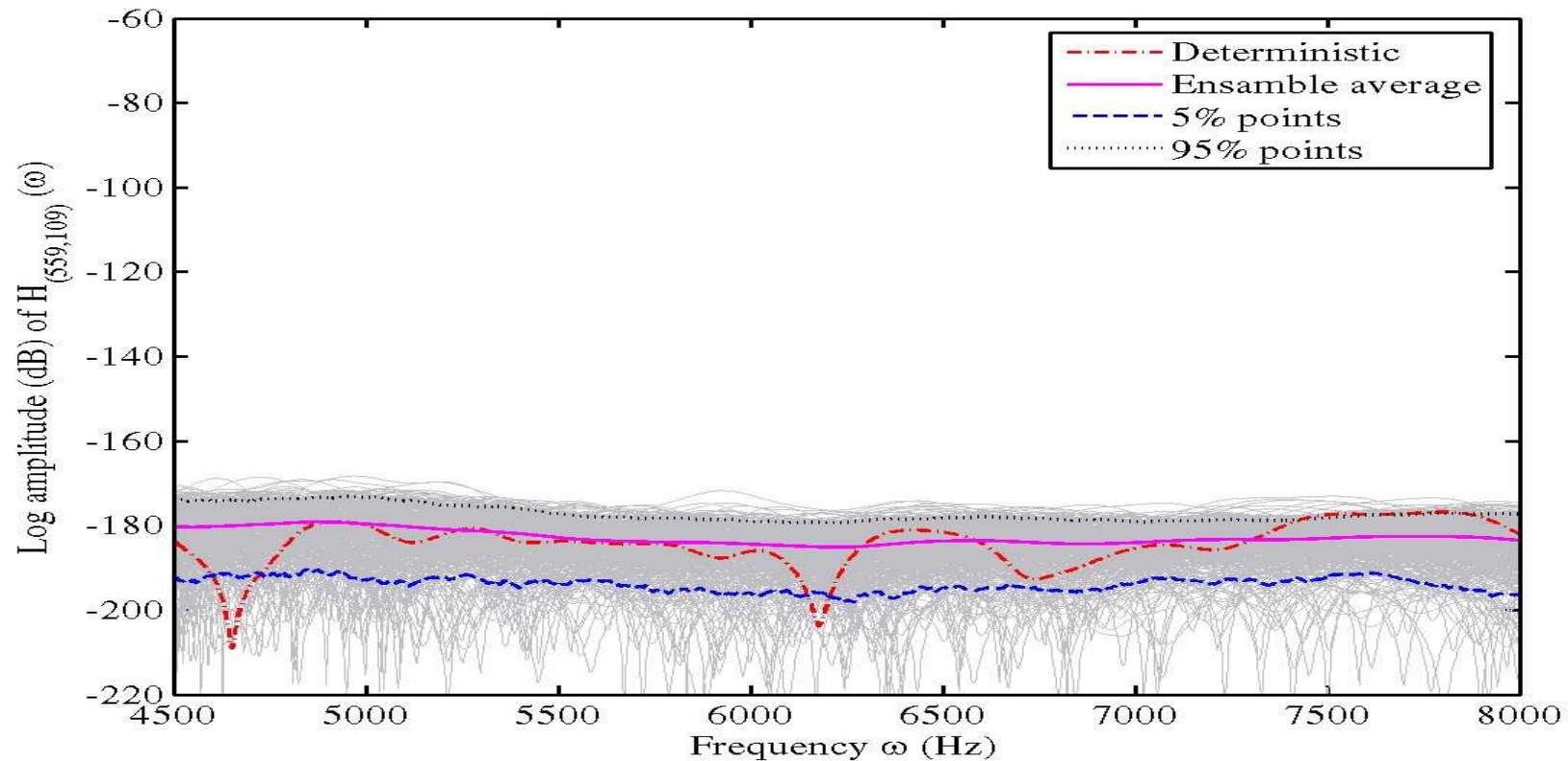


# SFEM cross-FRF: Mid Freq



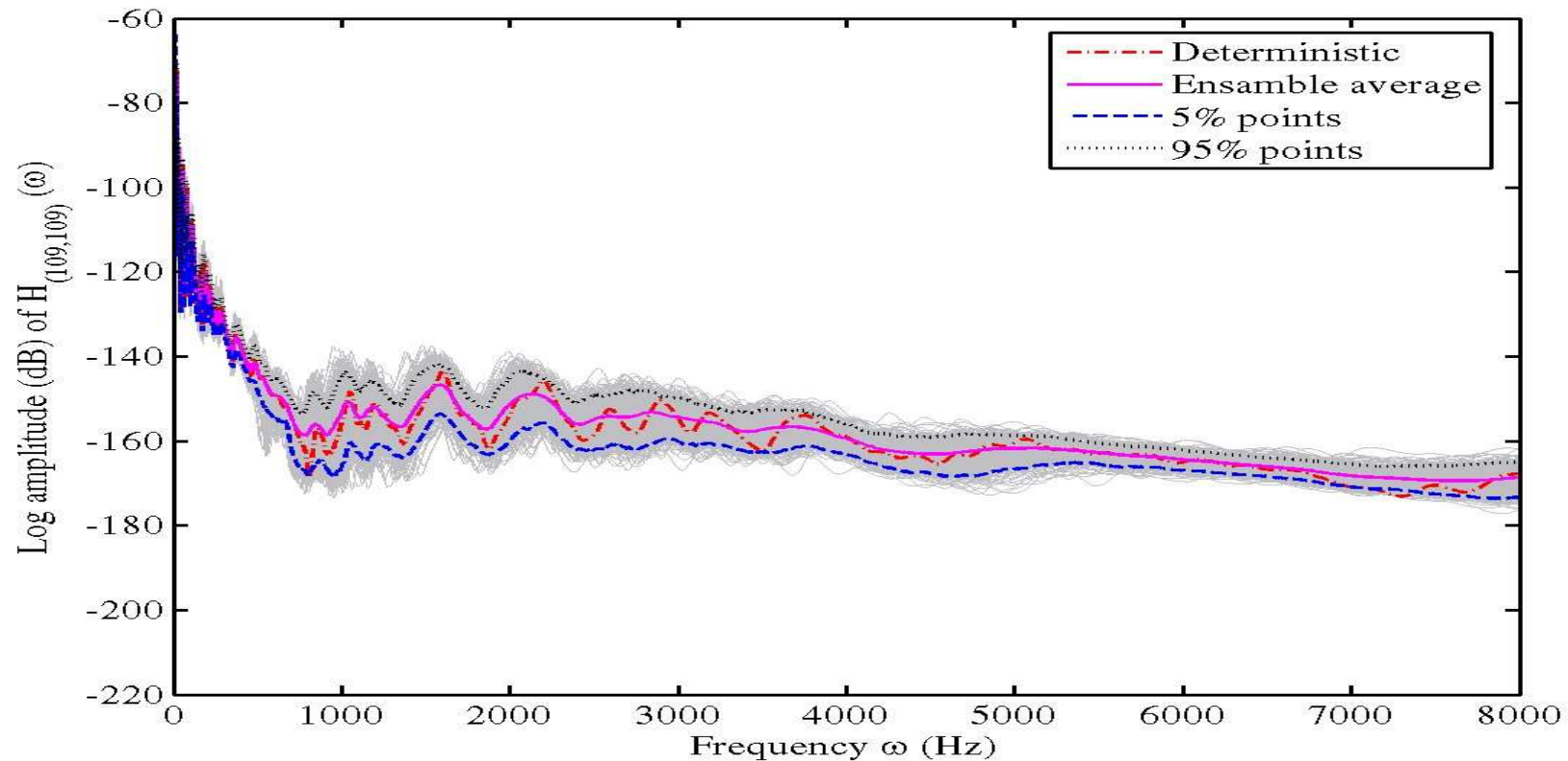
Direct stochastic finite-element Monte Carlo Simulation of the amplitude of the cross-FRF.

# SFEM cross-FRF: High Freq



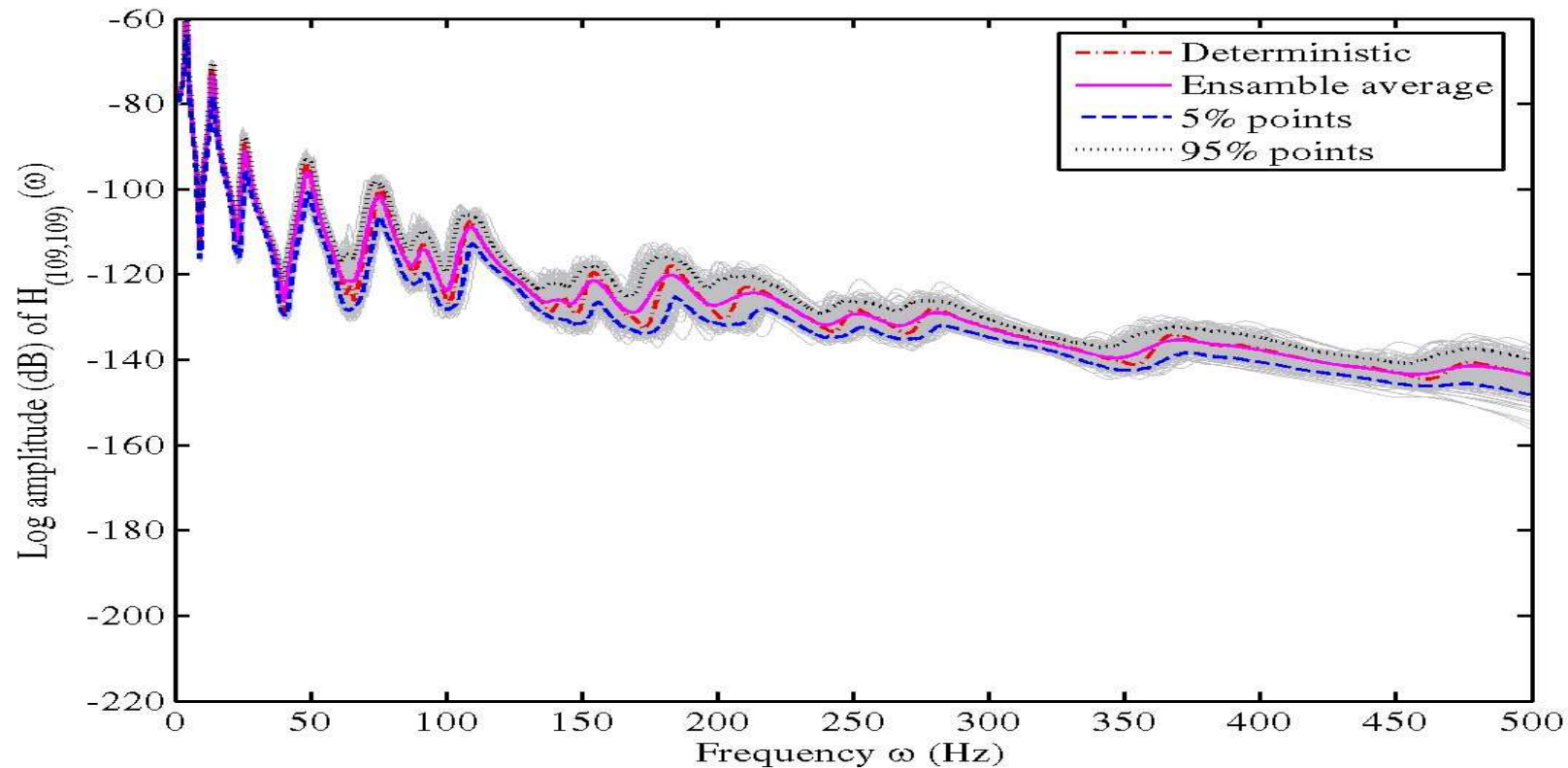
Direct stochastic finite-element Monte Carlo Simulation of the amplitude of the cross-FRF.

# SFEM driving-point-FRF



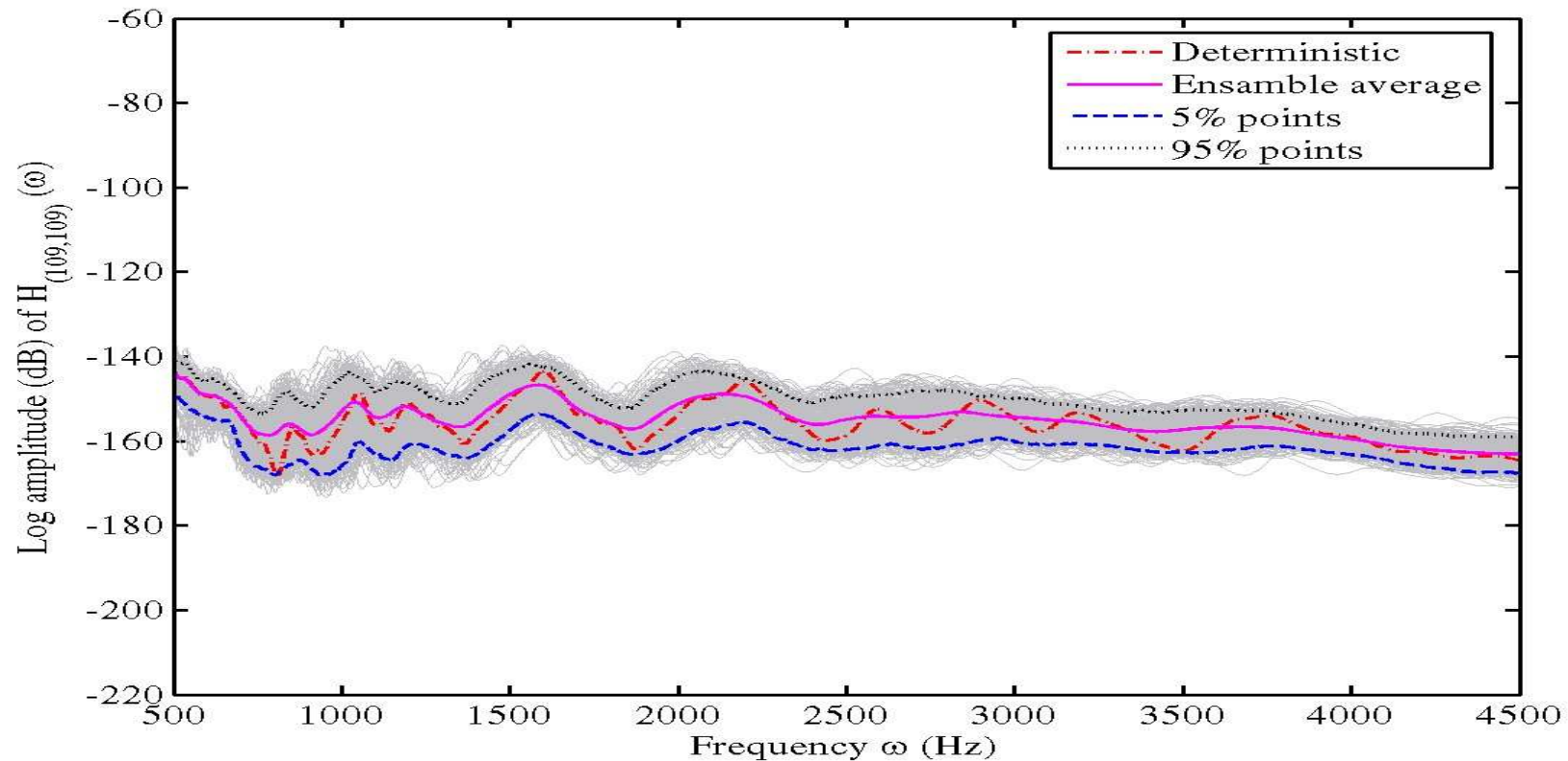
Direct stochastic finite-element Monte Carlo Simulation of the amplitude of the driving-point-FRF.

# SFEM driving-point-FRF: Low Freq



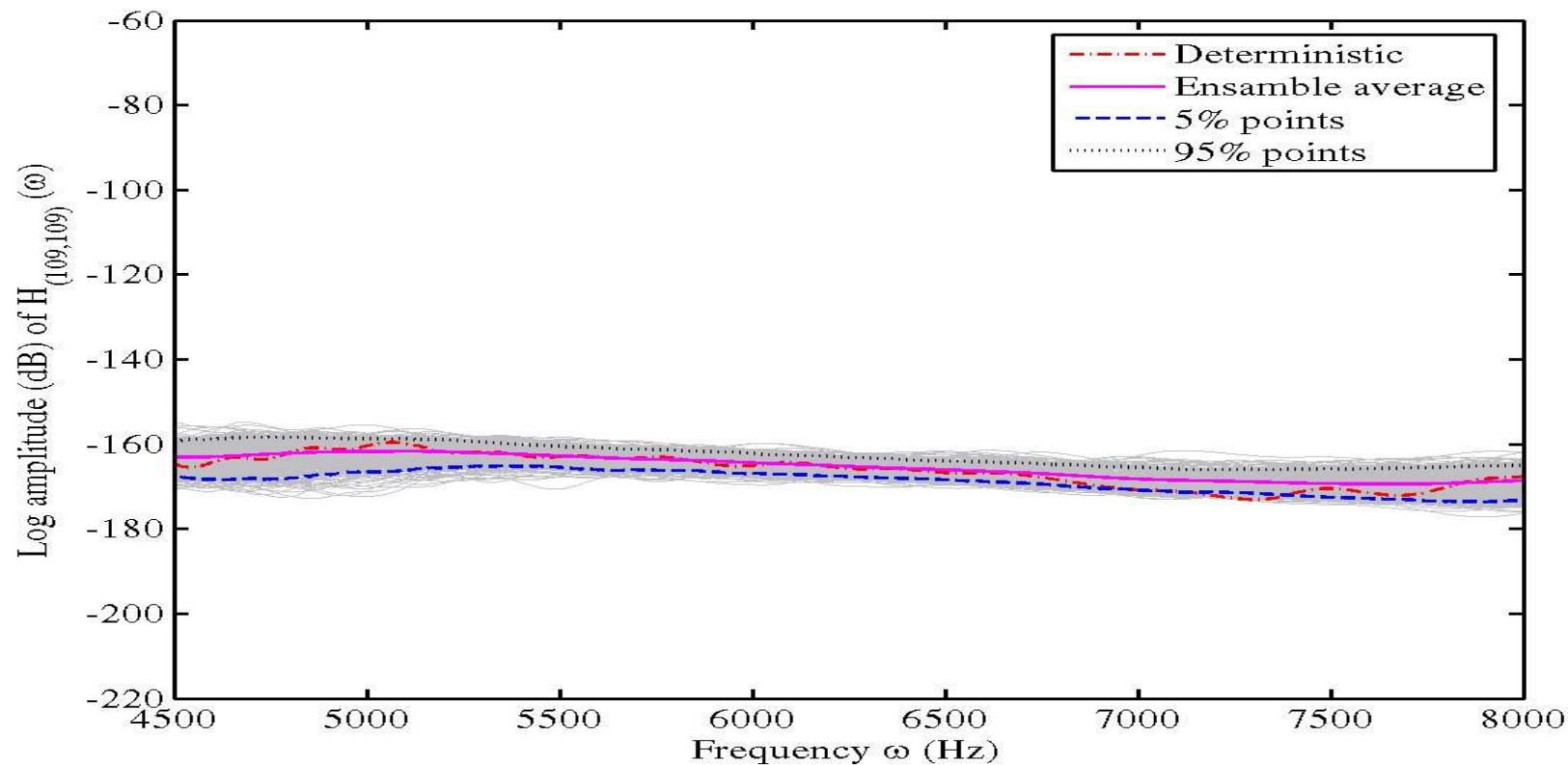
Direct stochastic finite-element Monte Carlo Simulation of the amplitude of the driving-point-FRF.

# SFEM driving-point-FRF: Mid Freq



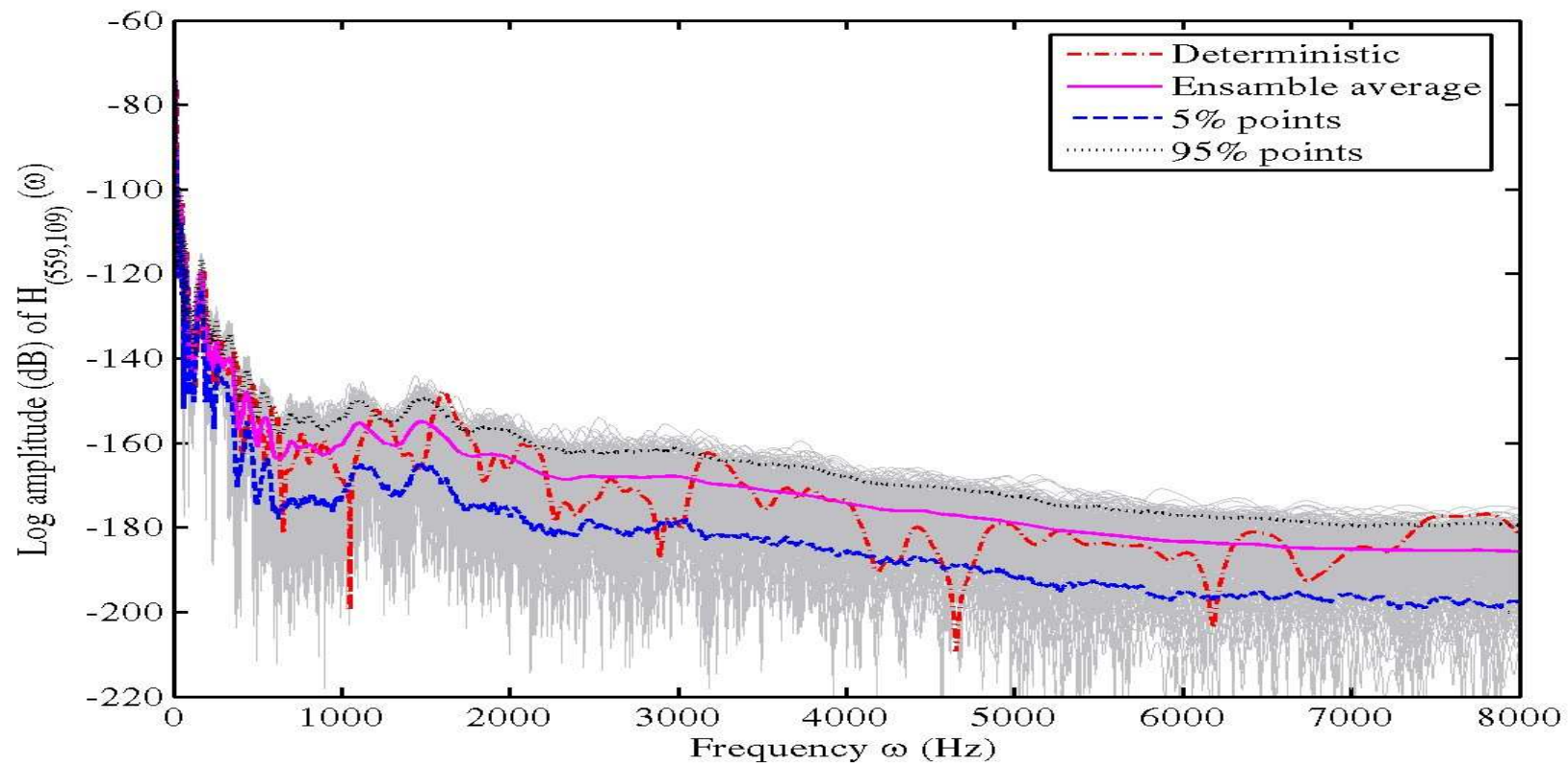
Direct stochastic finite-element Monte Carlo Simulation of the amplitude of the driving-point-FRF.

# SFEM driving-point-FRF: High Freq



Direct stochastic finite-element Monte Carlo Simulation of the amplitude of the driving-point-FRF.

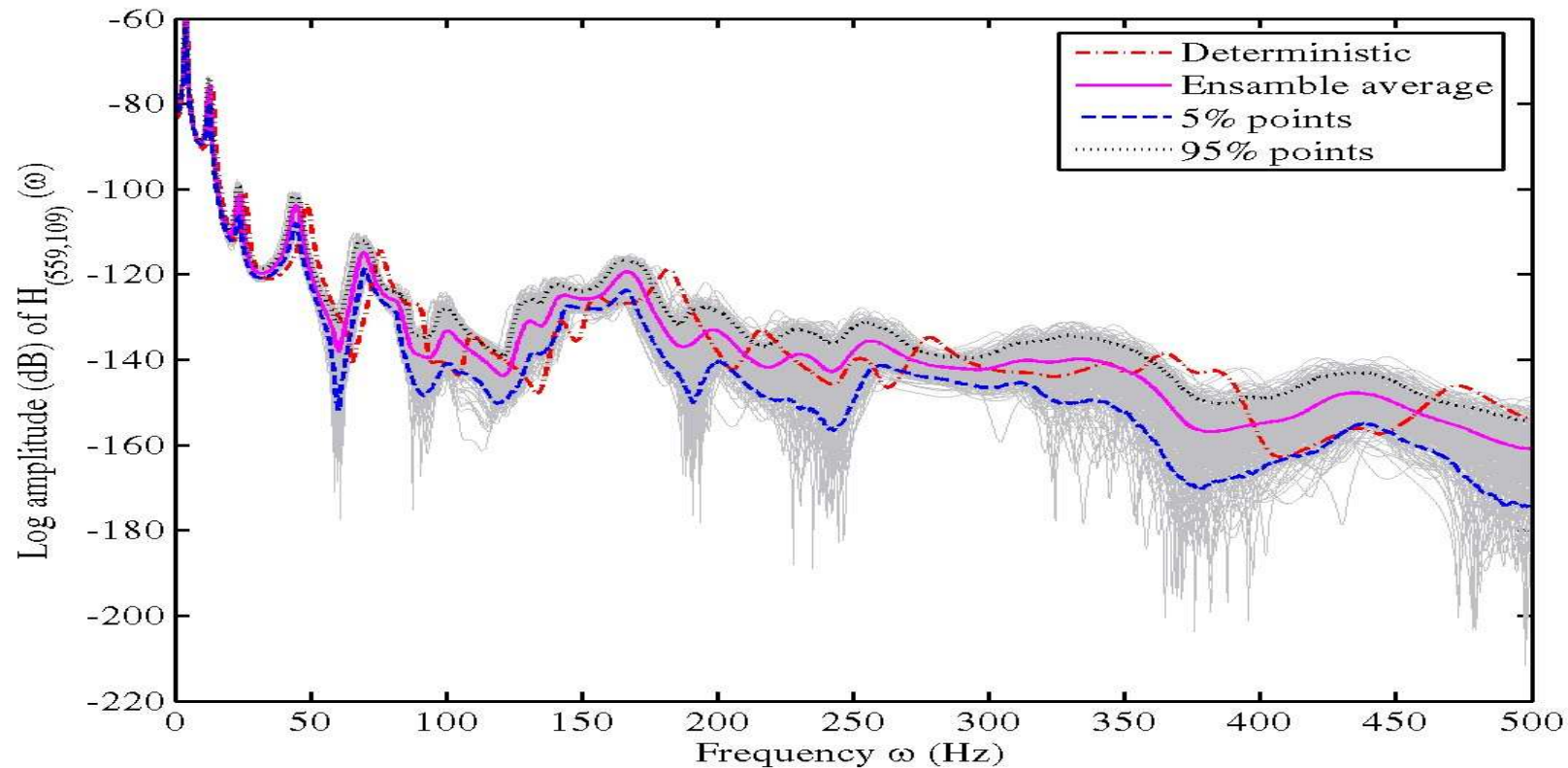
# RMT cross-FRF



Amplitude of the cross-FRF of the plate using optimal Wishart mass and stiffness matrices,

$$n = 702, \delta_M = 0.1166 \text{ and } \delta_K = 0.2622$$

# RMT cross-FRF: Low Freq

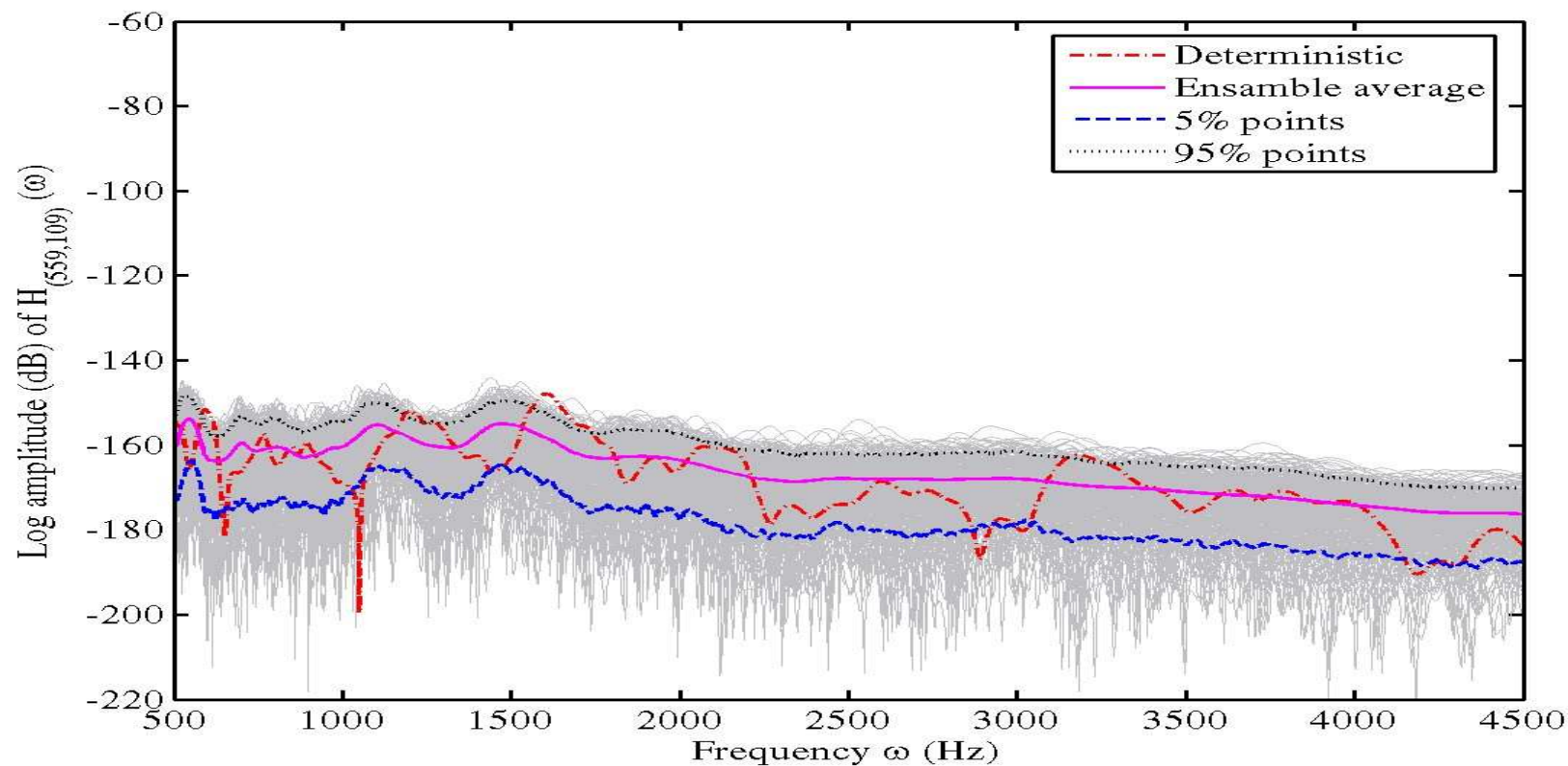


Amplitude of the cross-FRF of the plate using optimal Wishart mass and stiffness matrices,

$$n = 702, \delta_M = 0.1166 \text{ and } \delta_K = 0.2622$$



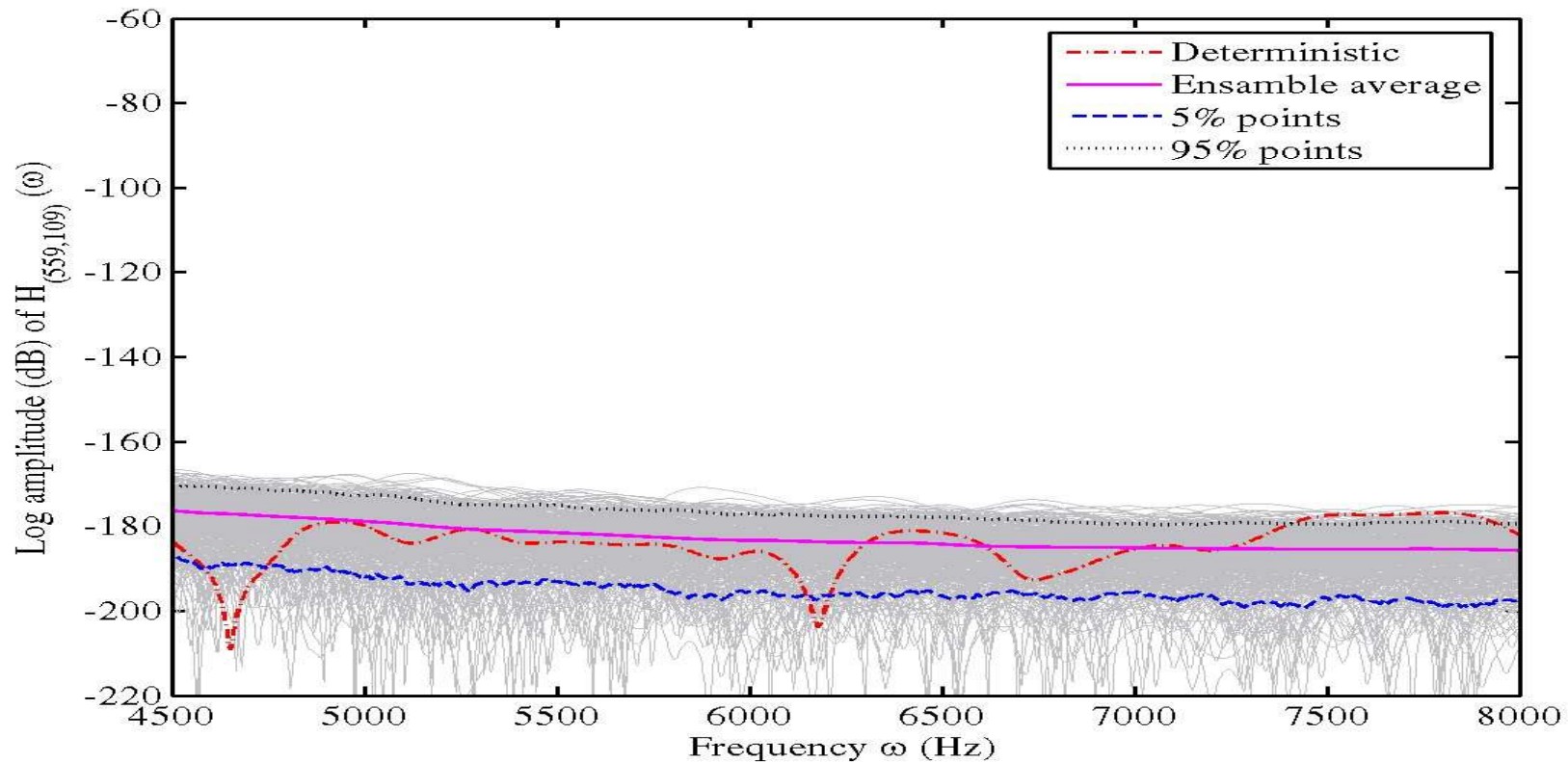
# RMT cross-FRF: Mid Freq



Amplitude of the cross-FRF of the plate using optimal Wishart mass and stiffness matrices,

$$n = 702, \delta_M = 0.1166 \text{ and } \delta_K = 0.2622$$

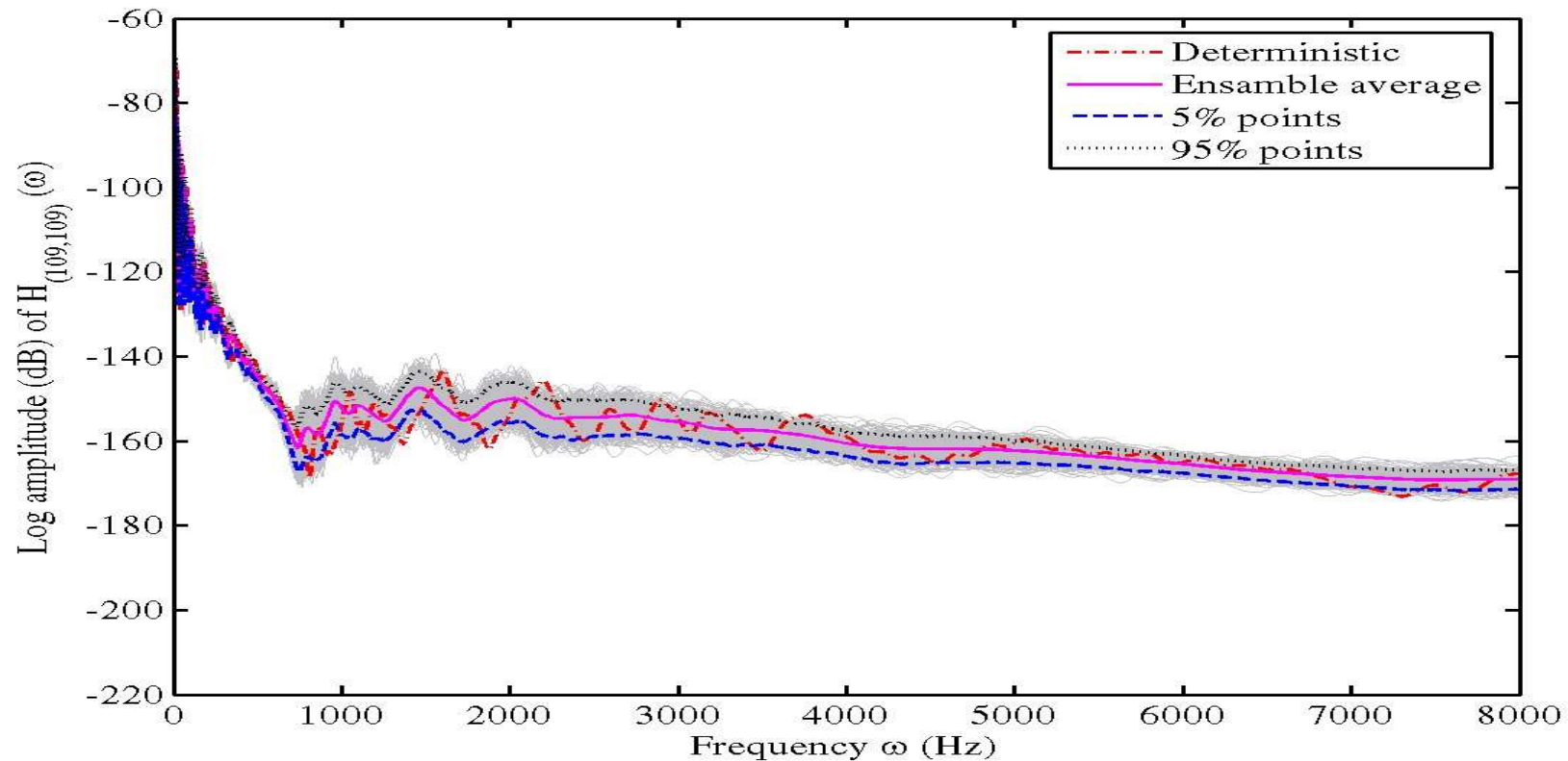
# RMT cross-FRF: High Freq



Amplitude of the cross-FRF of the plate using optimal Wishart mass and stiffness matrices,

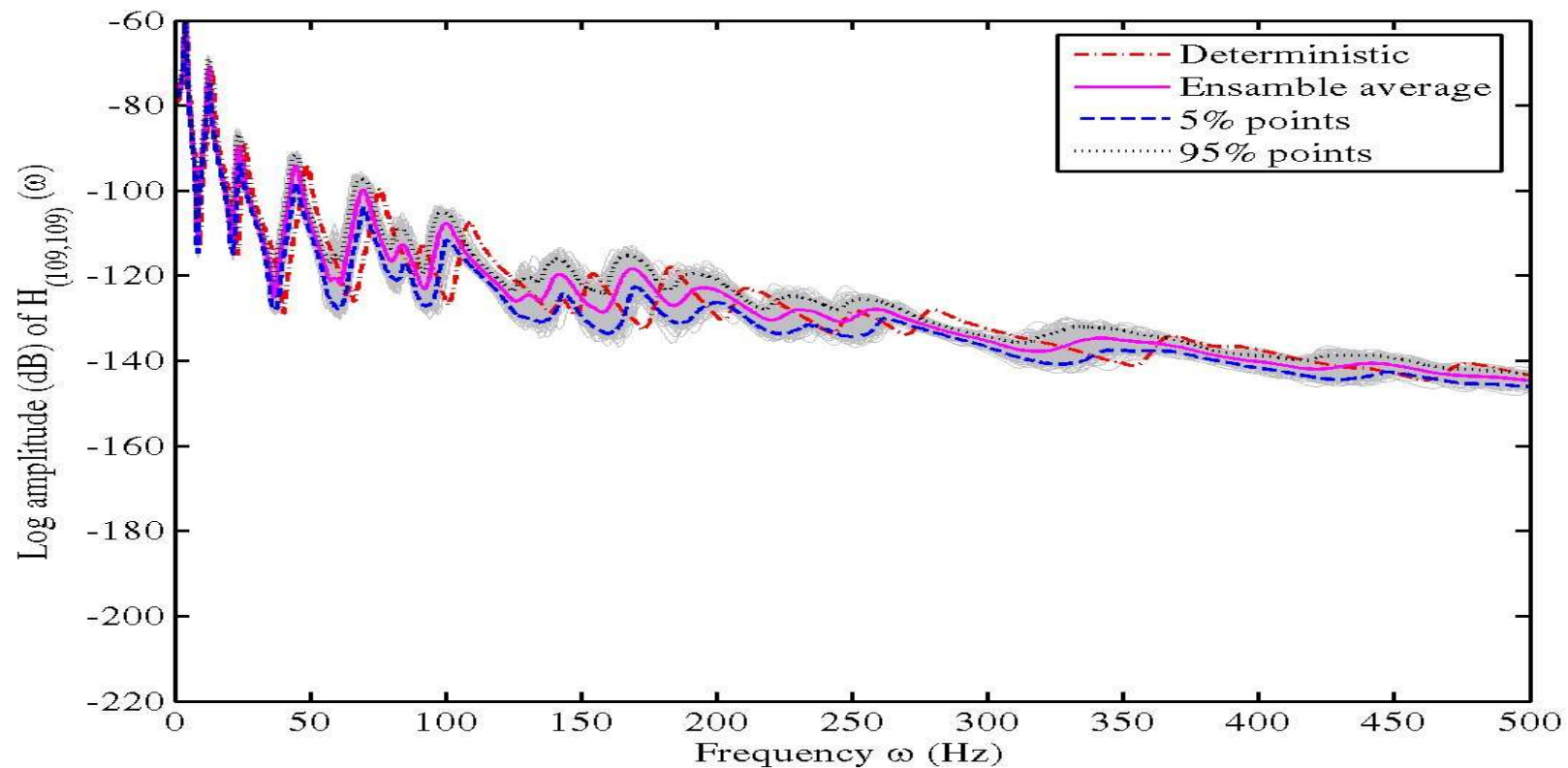
$$n = 702, \delta_M = 0.1166 \text{ and } \delta_K = 0.2622$$

# RMT driving-point-FRF



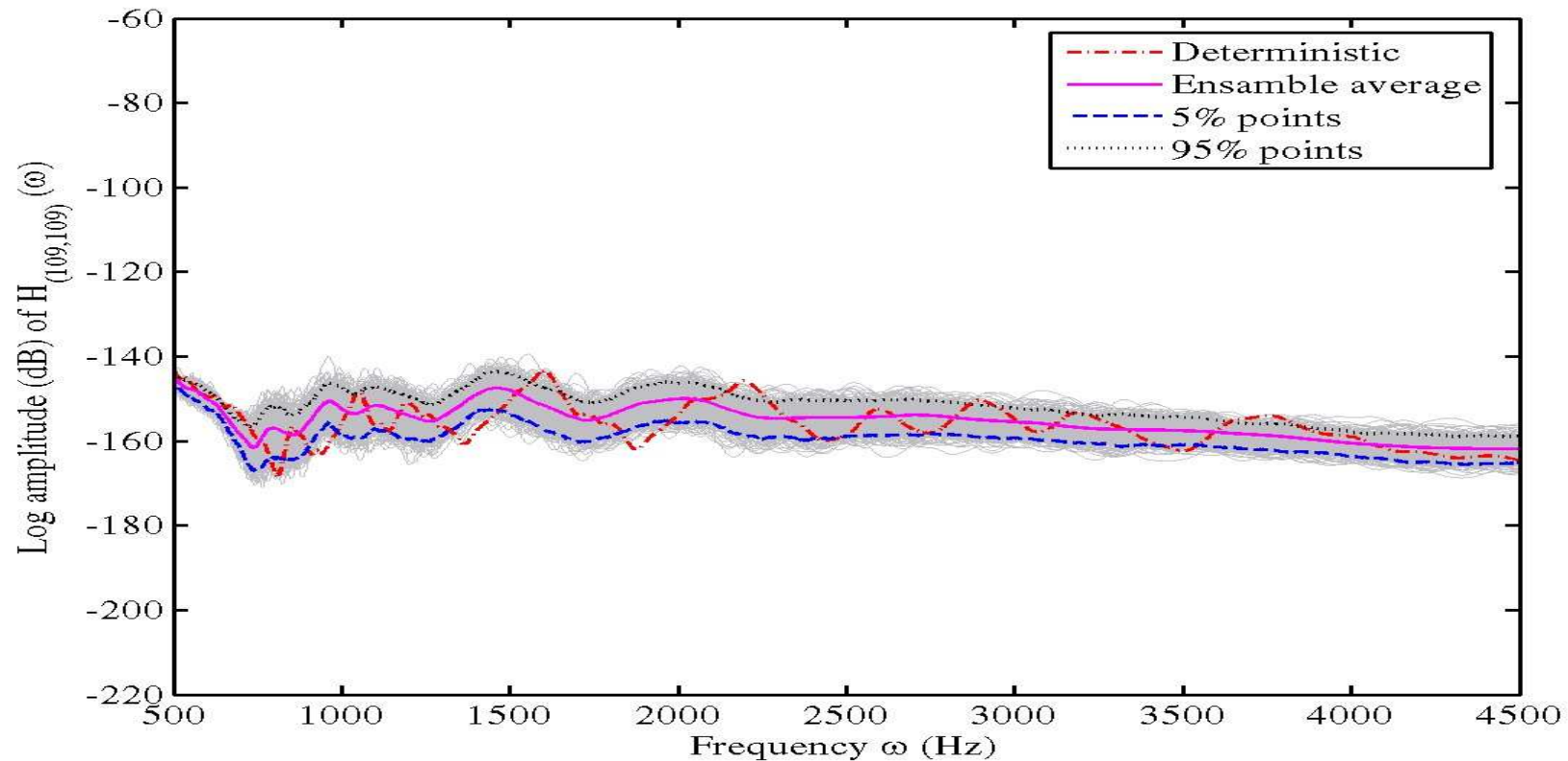
Amplitude of the driving-point-FRF of the plate using optimal Wishart mass and stiffness matrices,  $n = 702$ ,  $\delta_M = 0.1166$  and  $\delta_K = 0.2622$

# RMT driving-point-FRF: Low Freq



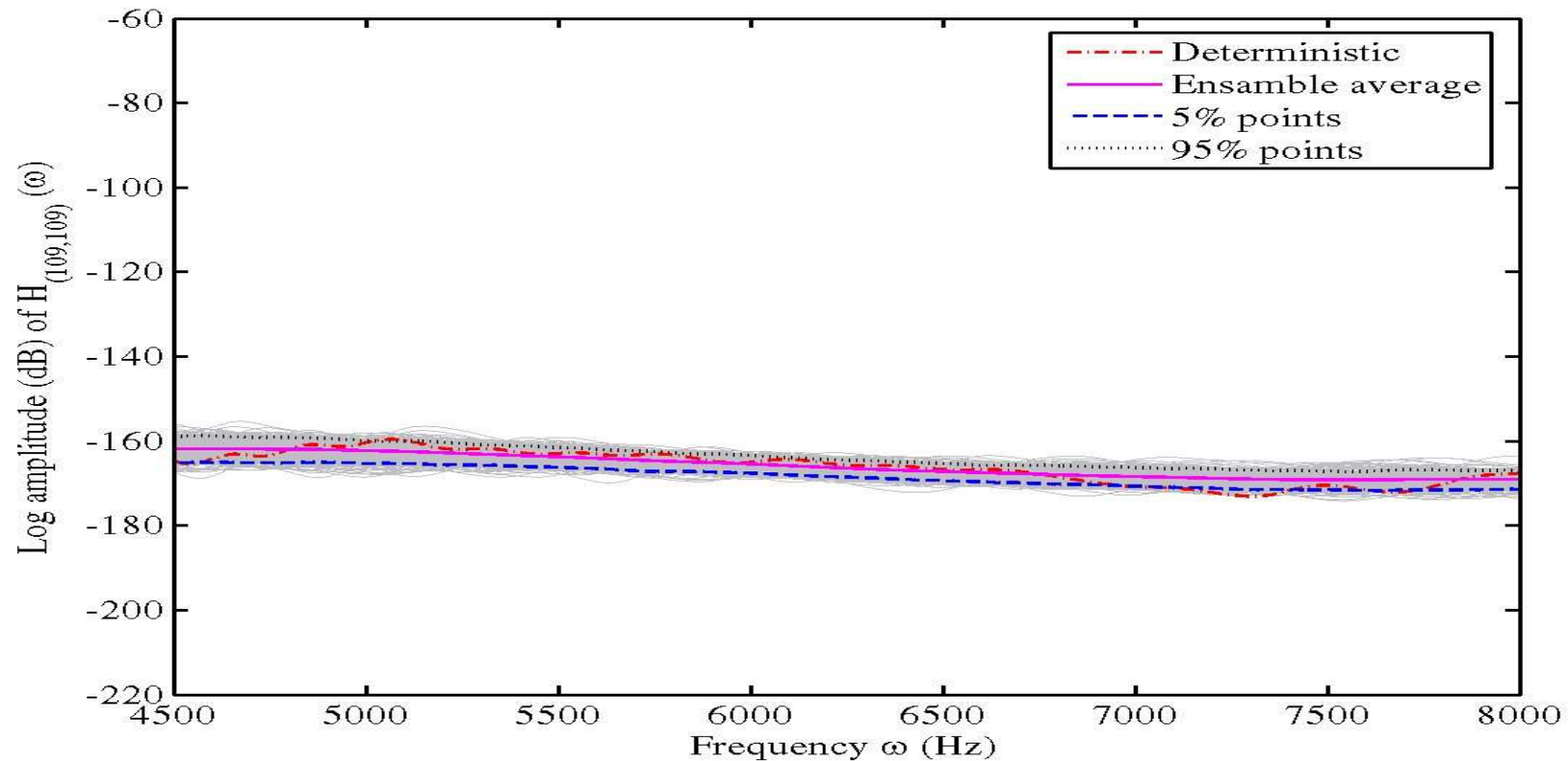
Amplitude of the driving-point-FRF of the plate using optimal Wishart mass and stiffness matrices,  $n = 702$ ,  $\delta_M = 0.1166$  and  $\delta_K = 0.2622$

# RMT driving-point-FRF: Mid Freq



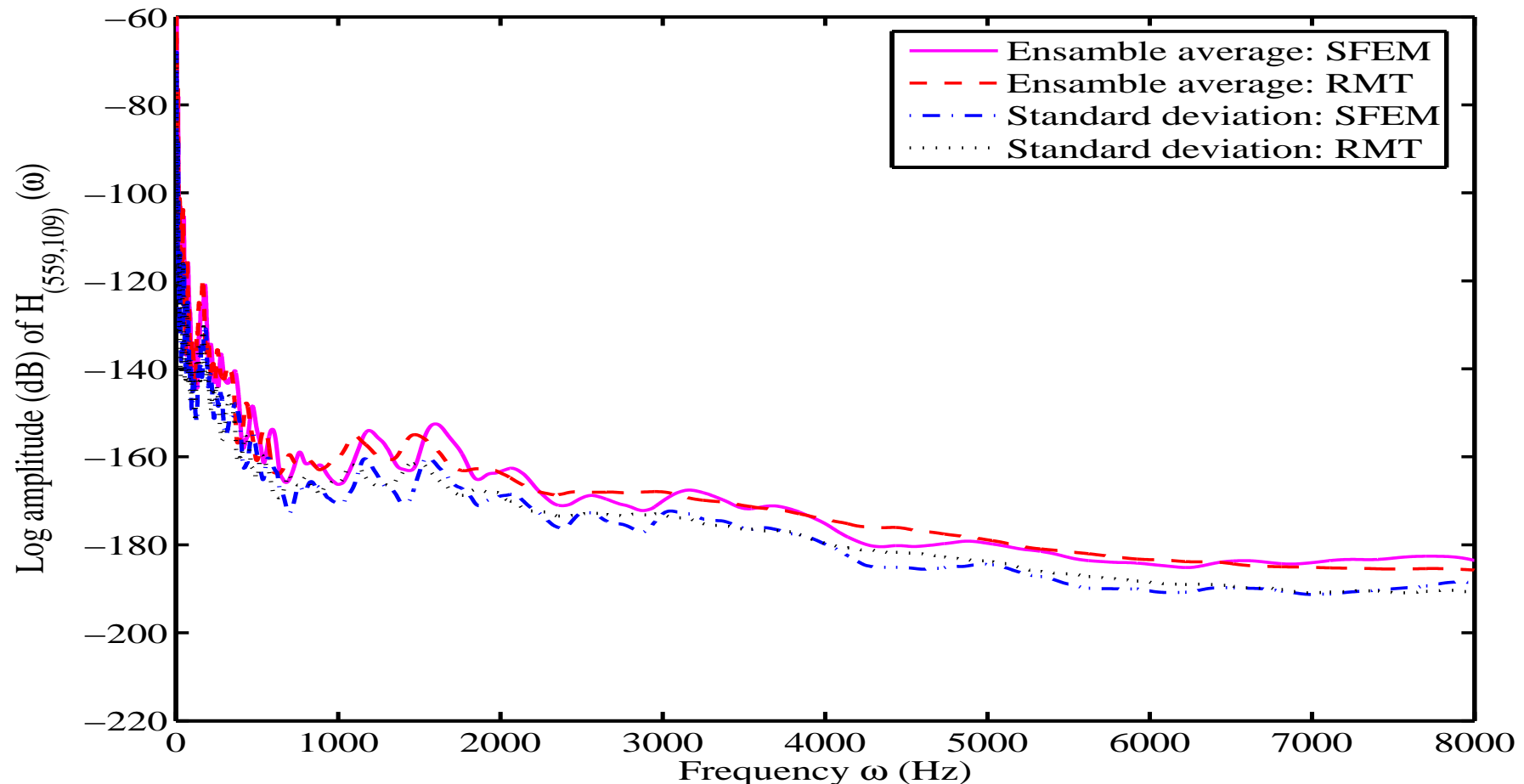
Amplitude of the driving-point-FRF of the plate using optimal Wishart mass and stiffness matrices,  $n = 702$ ,  $\delta_M = 0.1166$  and  $\delta_K = 0.2622$

# RMT driving-point-FRF: High Freq



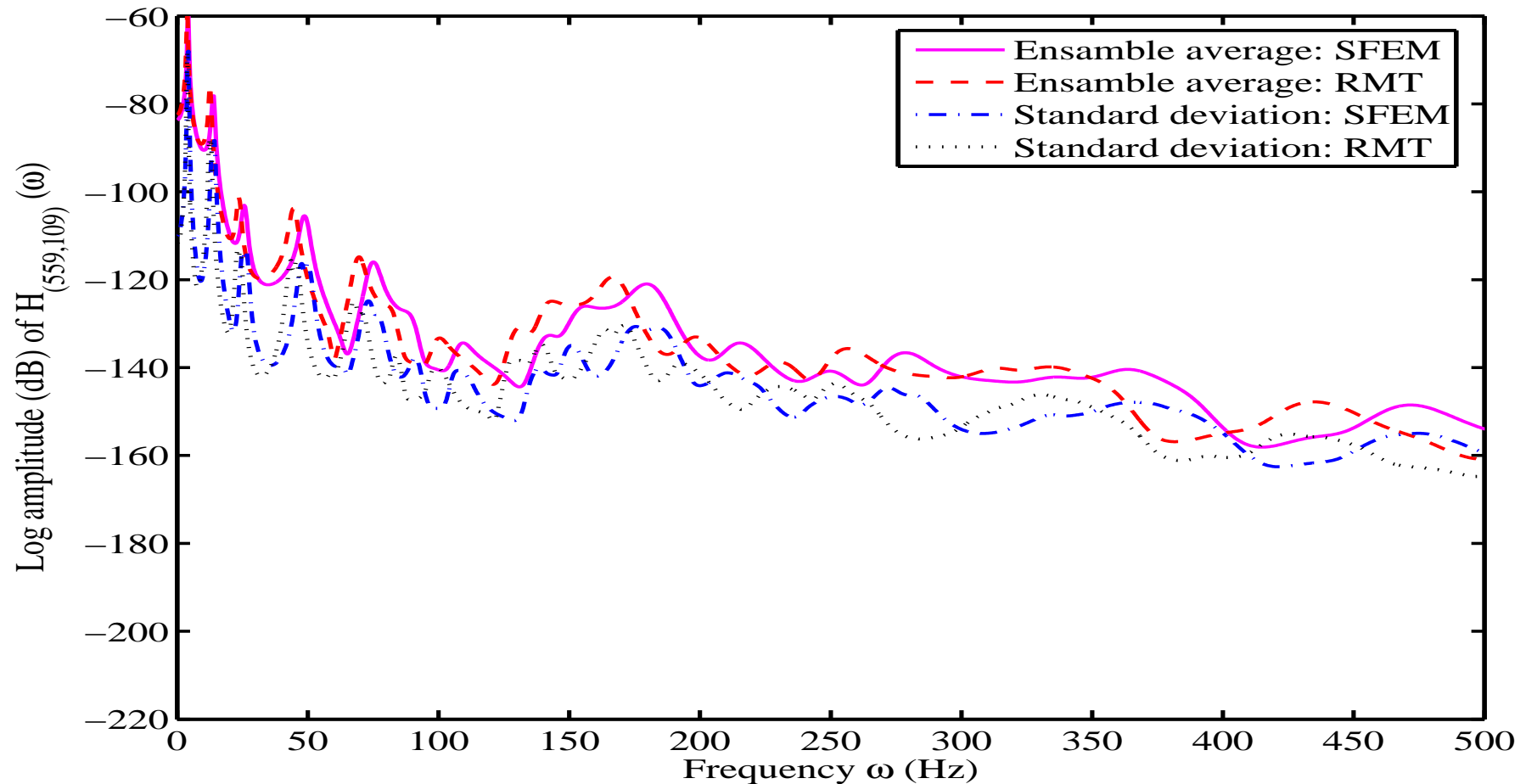
Amplitude of the driving-point-FRF of the plate using optimal Wishart mass and stiffness matrices,  $n = 702$ ,  $\delta_M = 0.1166$  and  $\delta_K = 0.2622$

# Comparison of cross-FRF



Comparison of the mean and standard deviation of the amplitude of the cross-FRF.

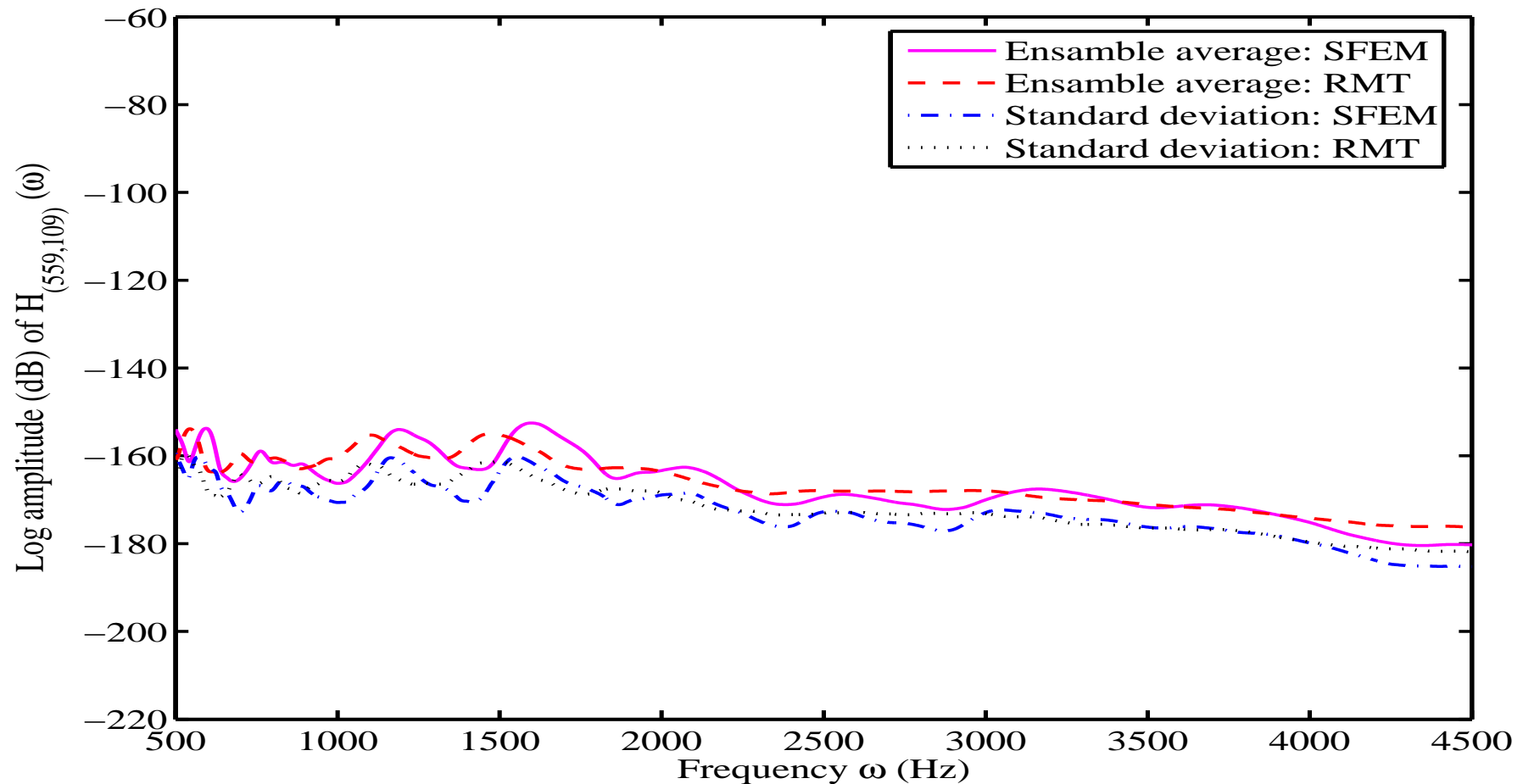
# Comparison of cross-FRF: Low Freq



Comparison of the mean and standard deviation of the amplitude of the cross-FRF.

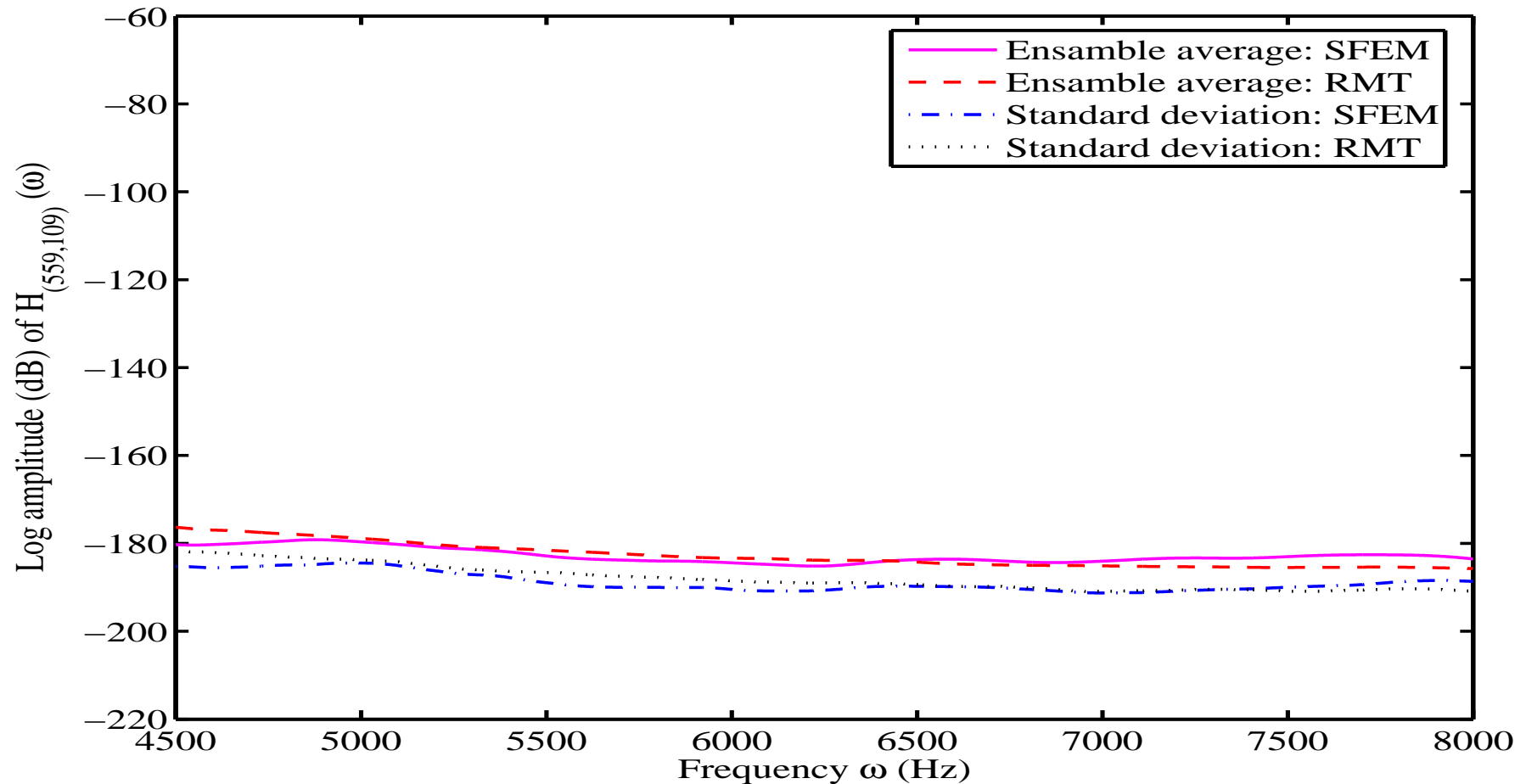


# Comparison of cross-FRF: Mid Freq



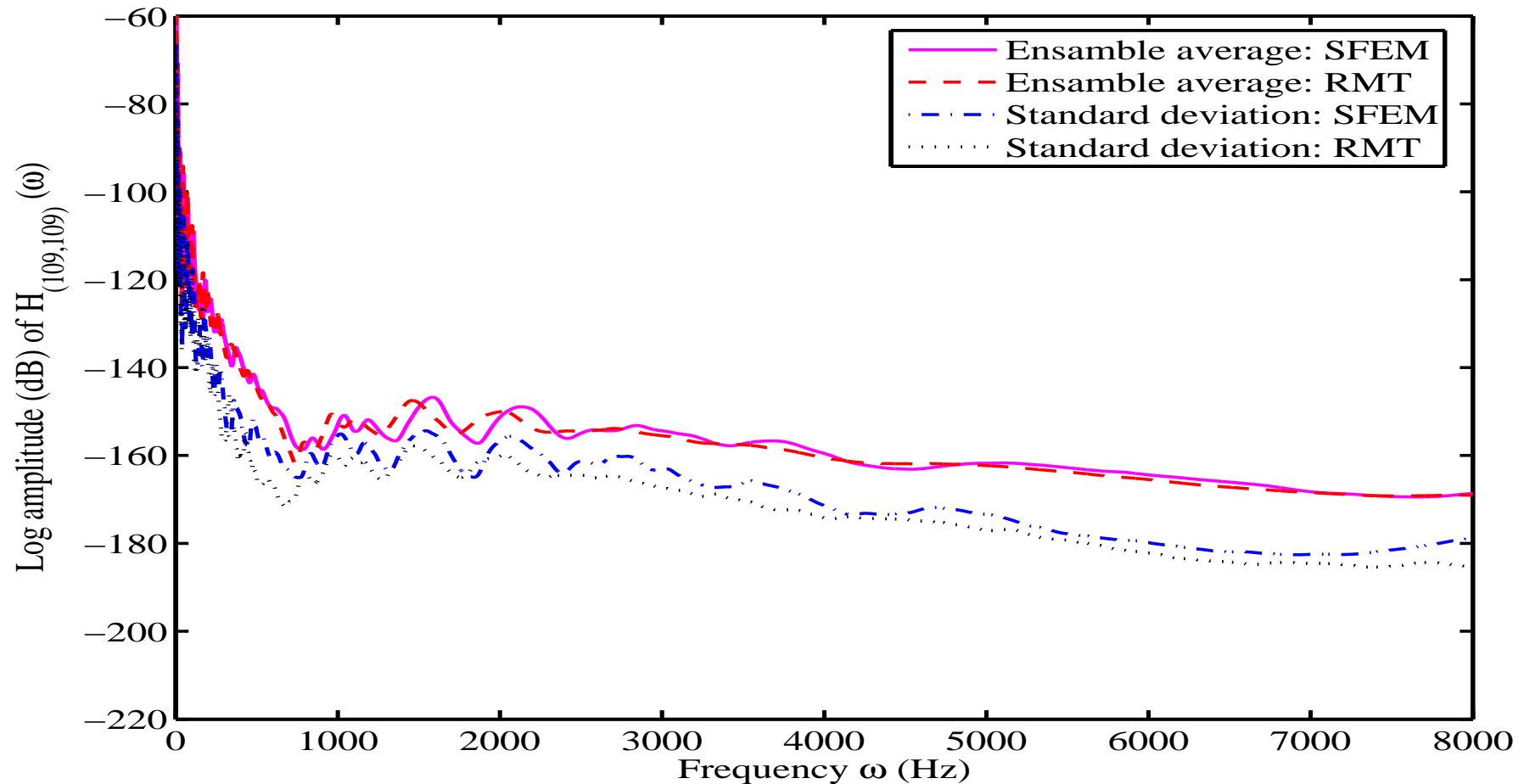
Comparison of the mean and standard deviation of the amplitude of the cross-FRF.

# Comparison of cross-FRF: High Freq



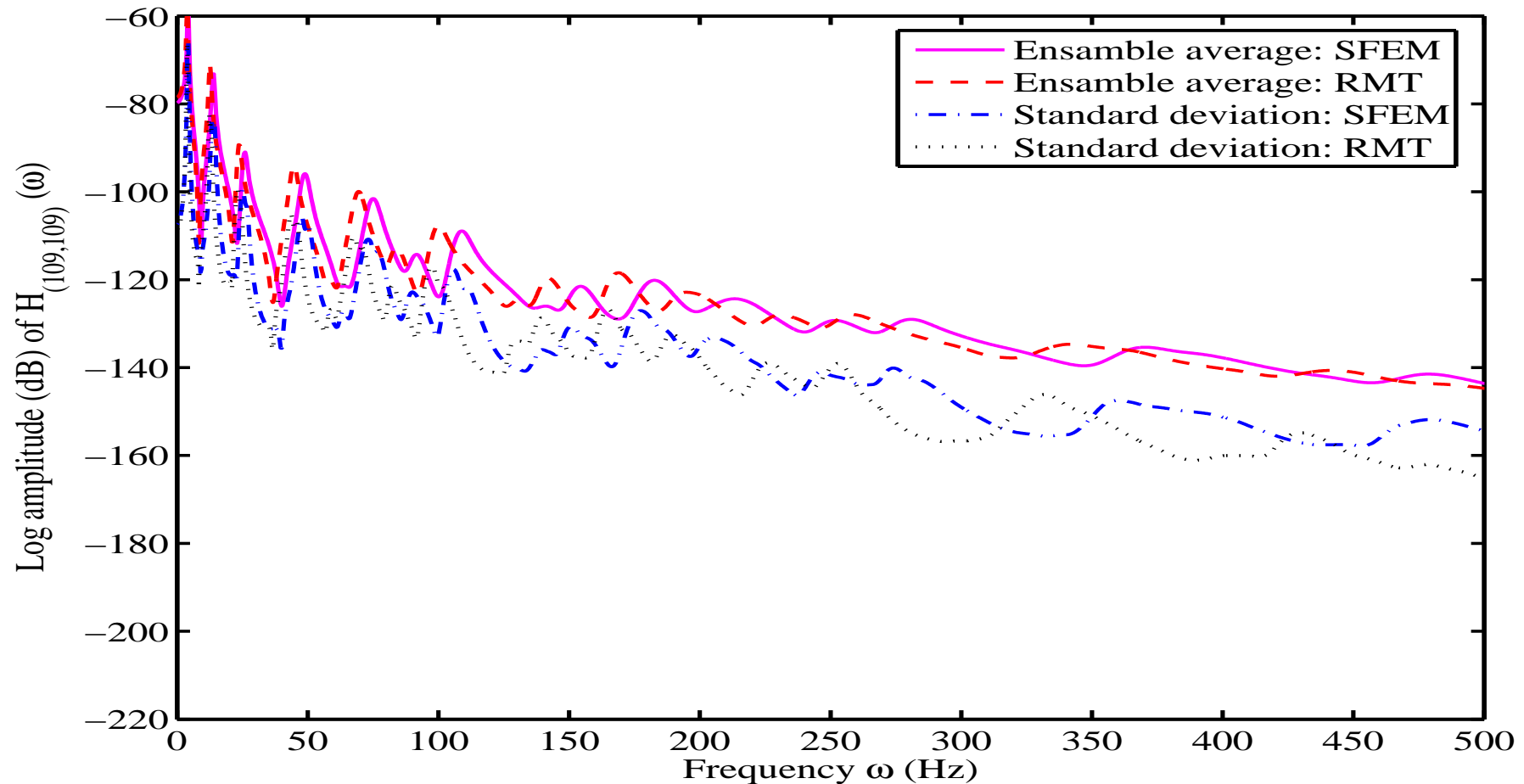
Comparison of the mean and standard deviation of the amplitude of the cross-FRF.

# Comparison of driving-point-FRF



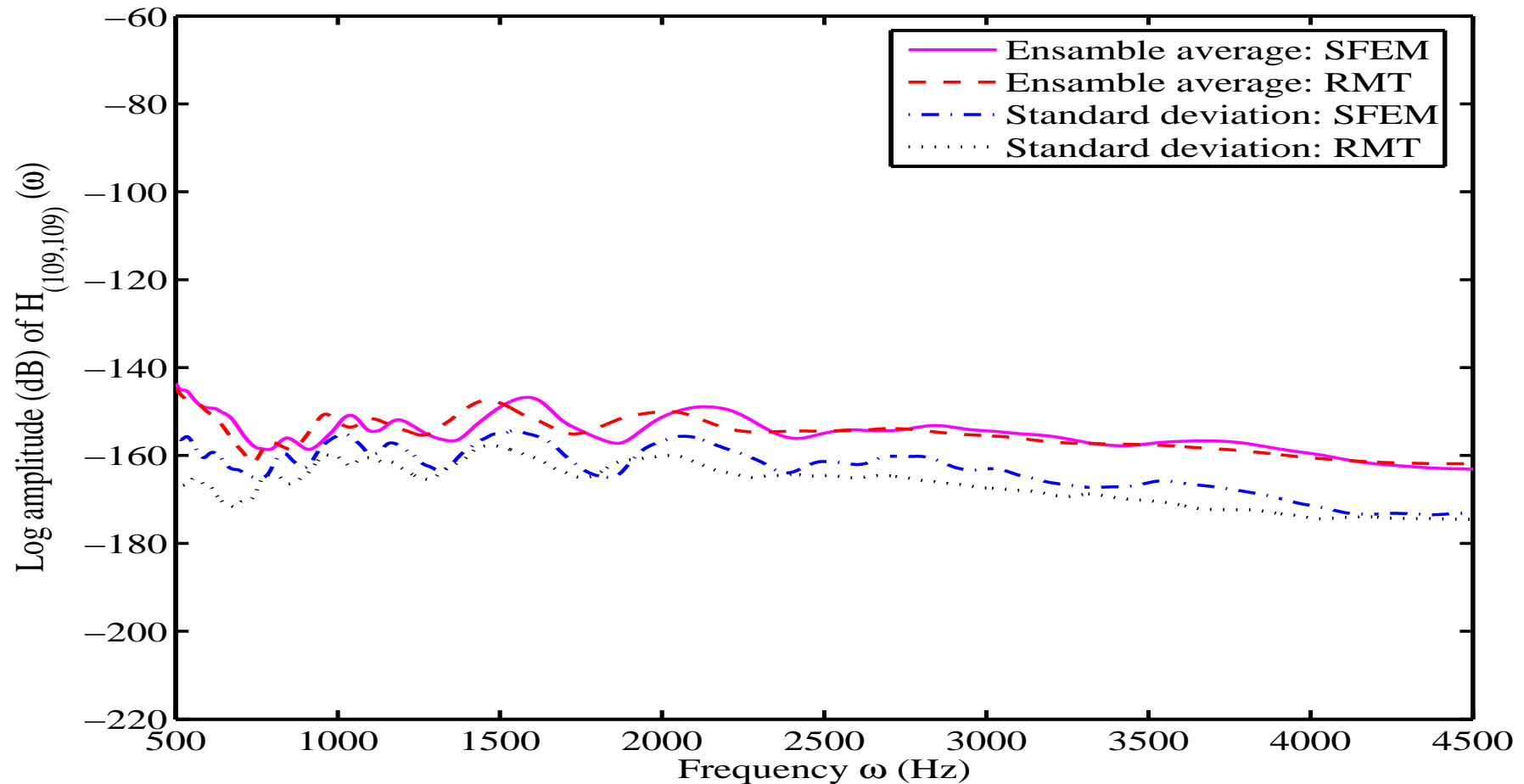
Comparison of the mean and standard deviation of the amplitude of the driving-point-FRF.

# Comparison of driving-point-FRF: Low Freq



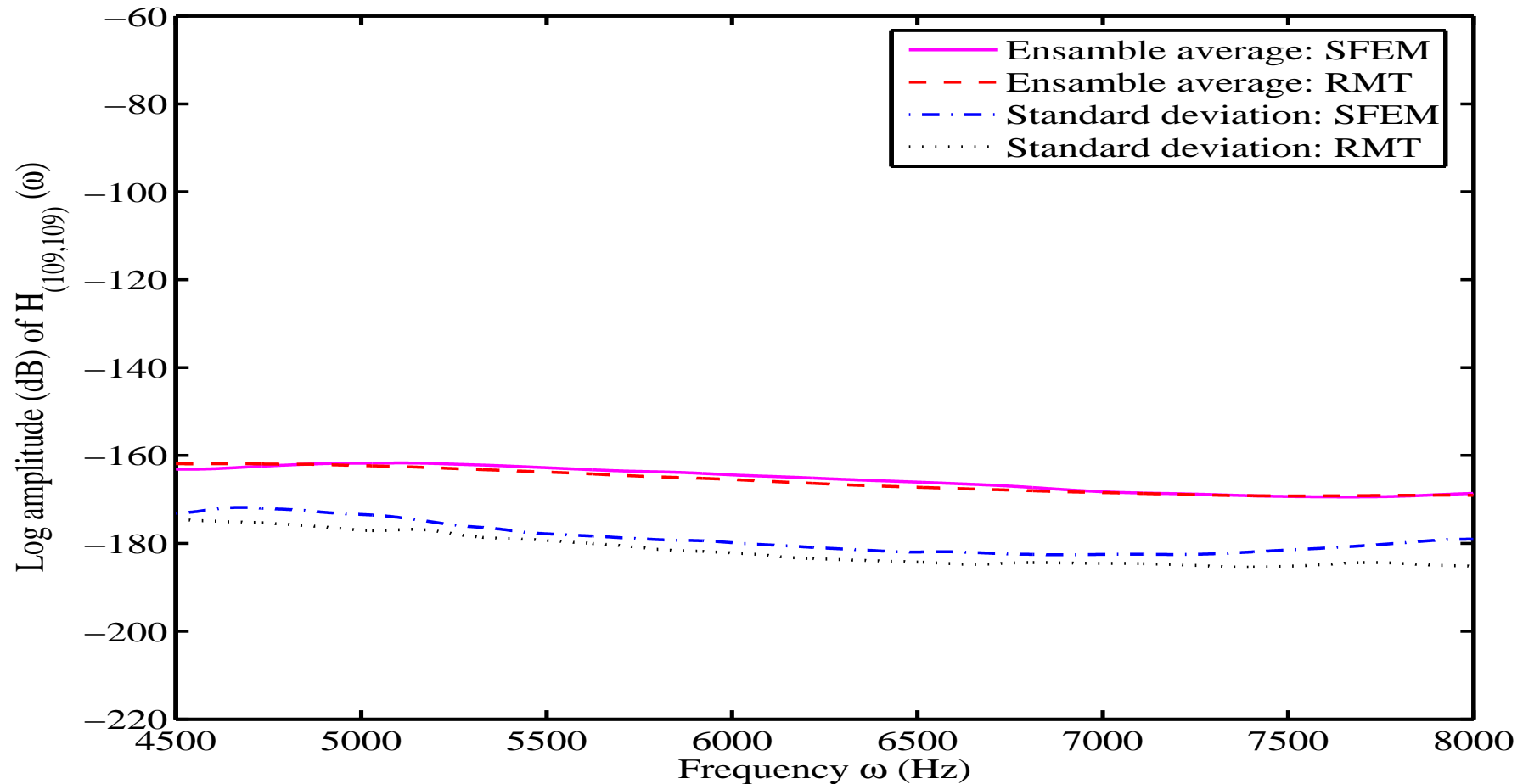
Comparison of the mean and standard deviation of the amplitude of the driving-point-FRF.

# Comparison of driving-point-FRF: Mid Freq



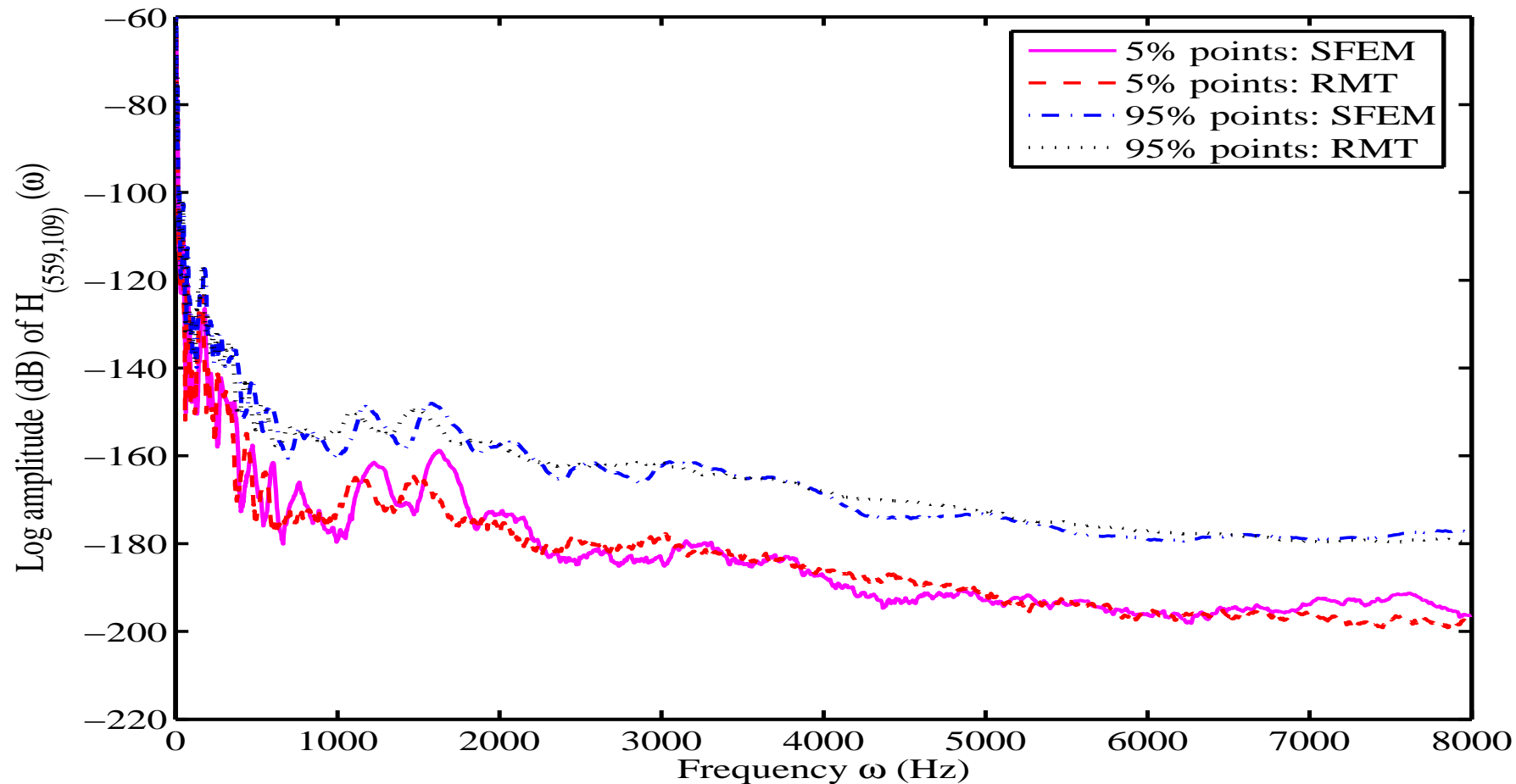
Comparison of the mean and standard deviation of the amplitude of the driving-point-FRF.

# Comparison of driving-point-FRF: High Freq



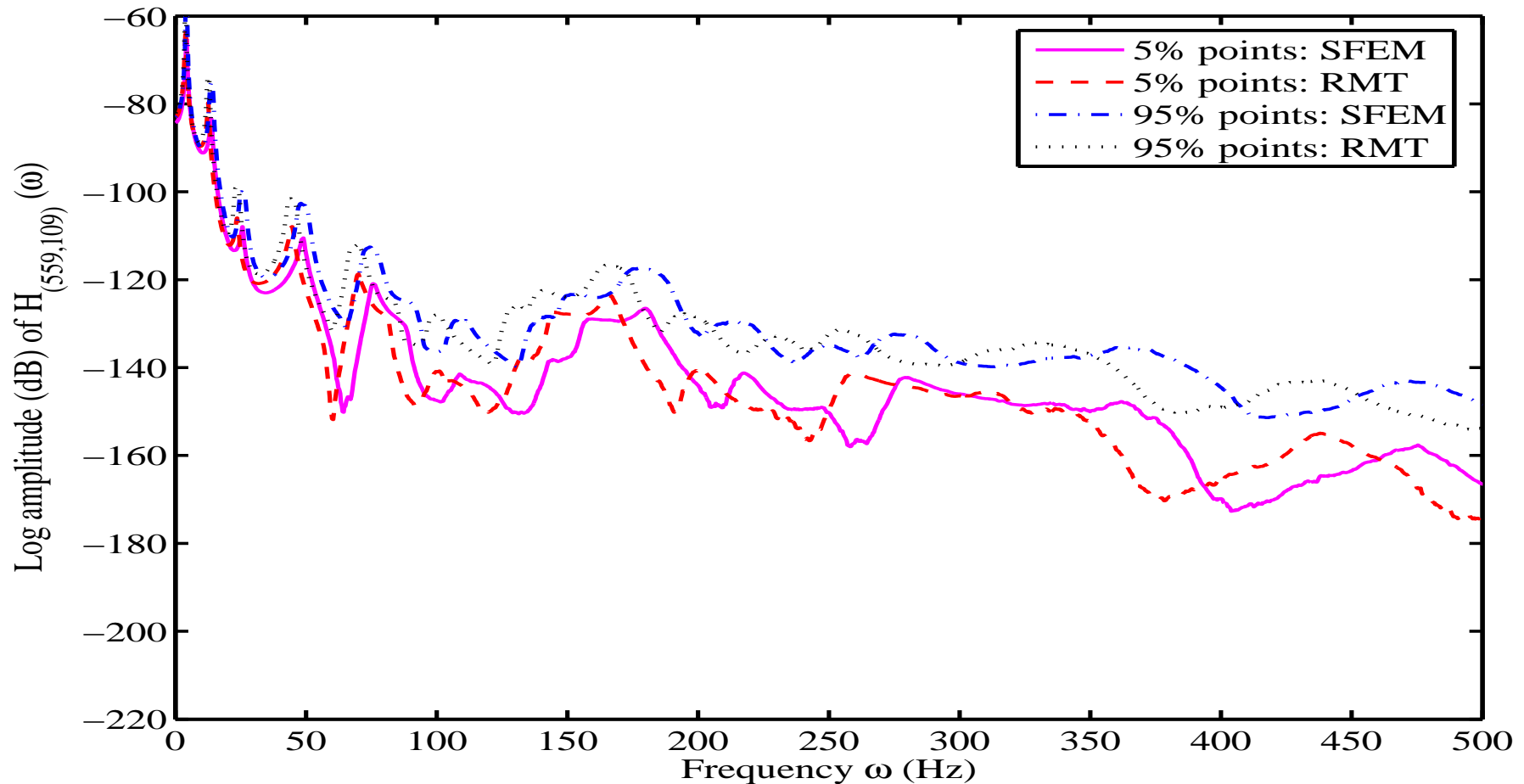
Comparison of the mean and standard deviation of the amplitude of the driving-point-FRF.

# Comparison of cross-FRF



Comparison of the 5% and 95% probability points of the amplitude of the cross-FRF.

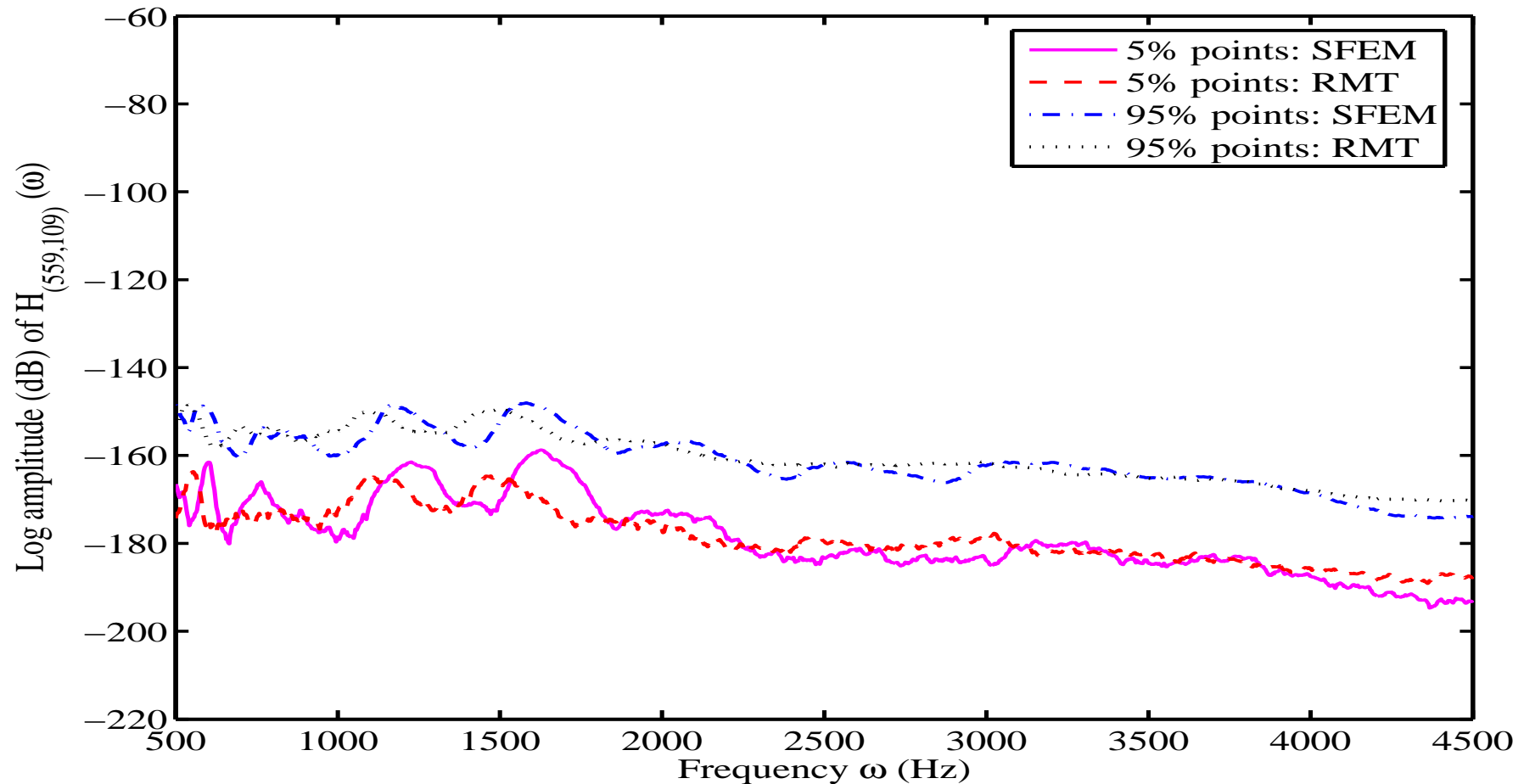
# Comparison of cross-FRF: Low Freq



Comparison of the 5% and 95% probability points of the amplitude of the cross-FRF.

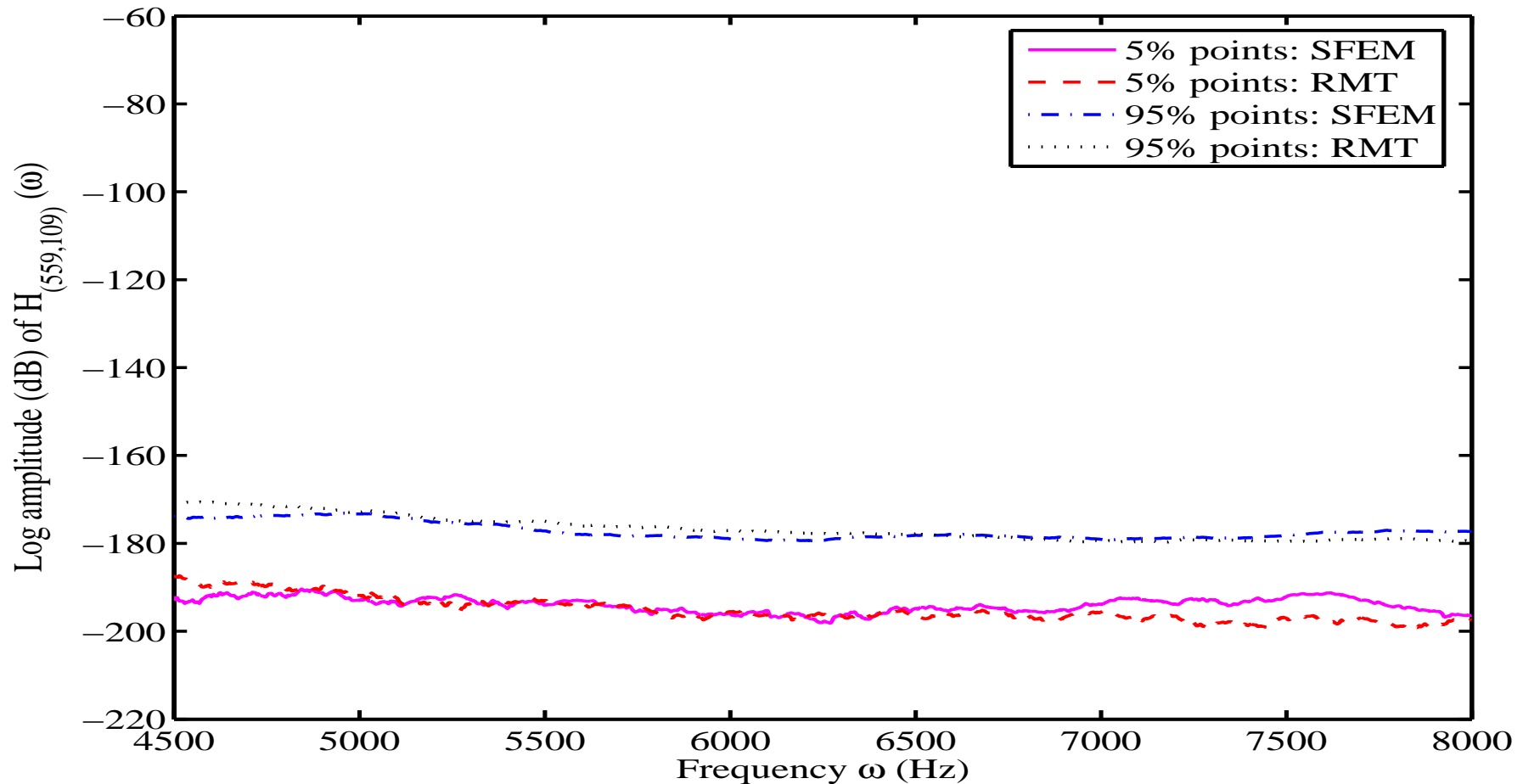


# Comparison of cross-FRF: Mid Freq



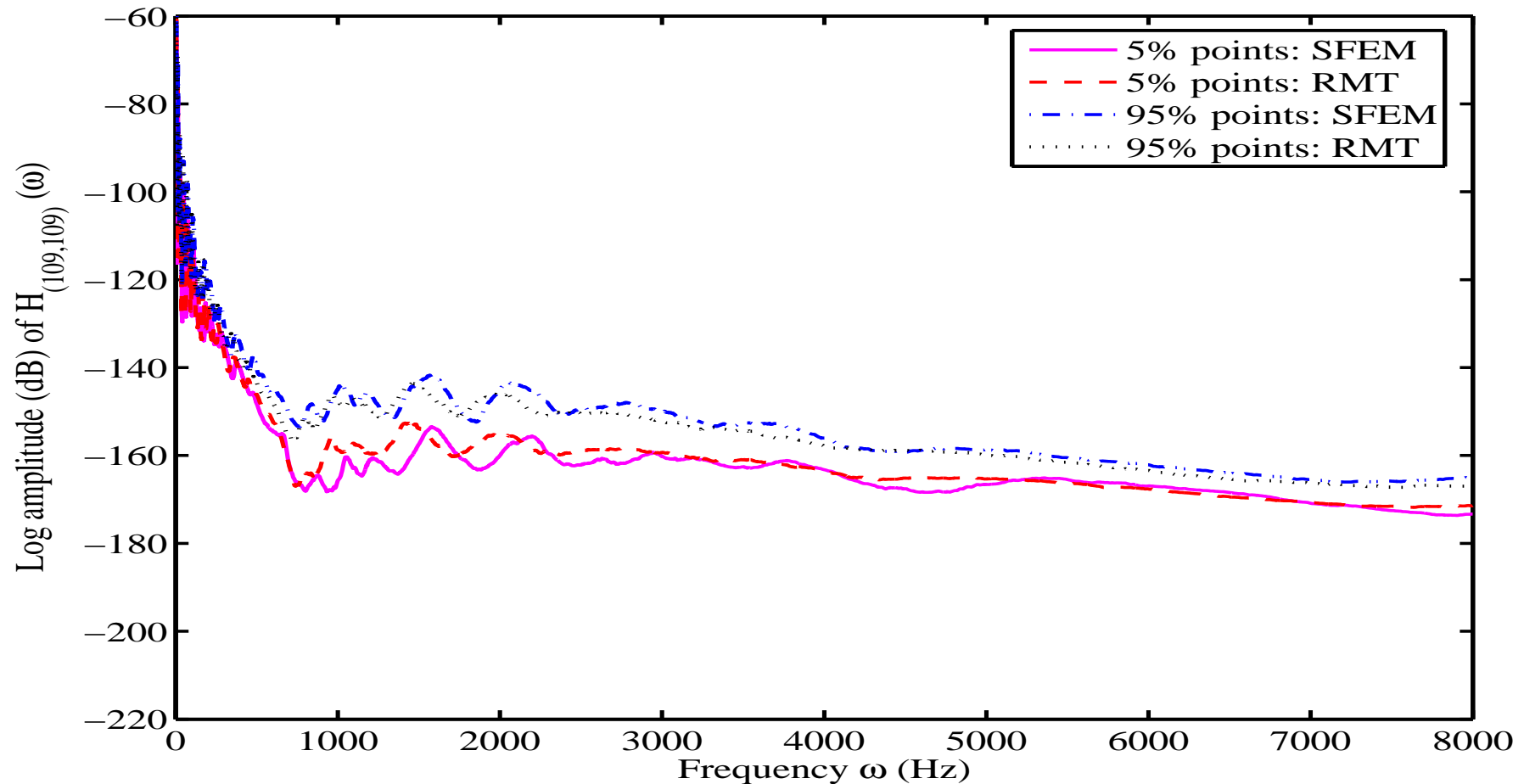
Comparison of the 5% and 95% probability points of the amplitude of the cross-FRF.

# Comparison of cross-FRF: High Freq



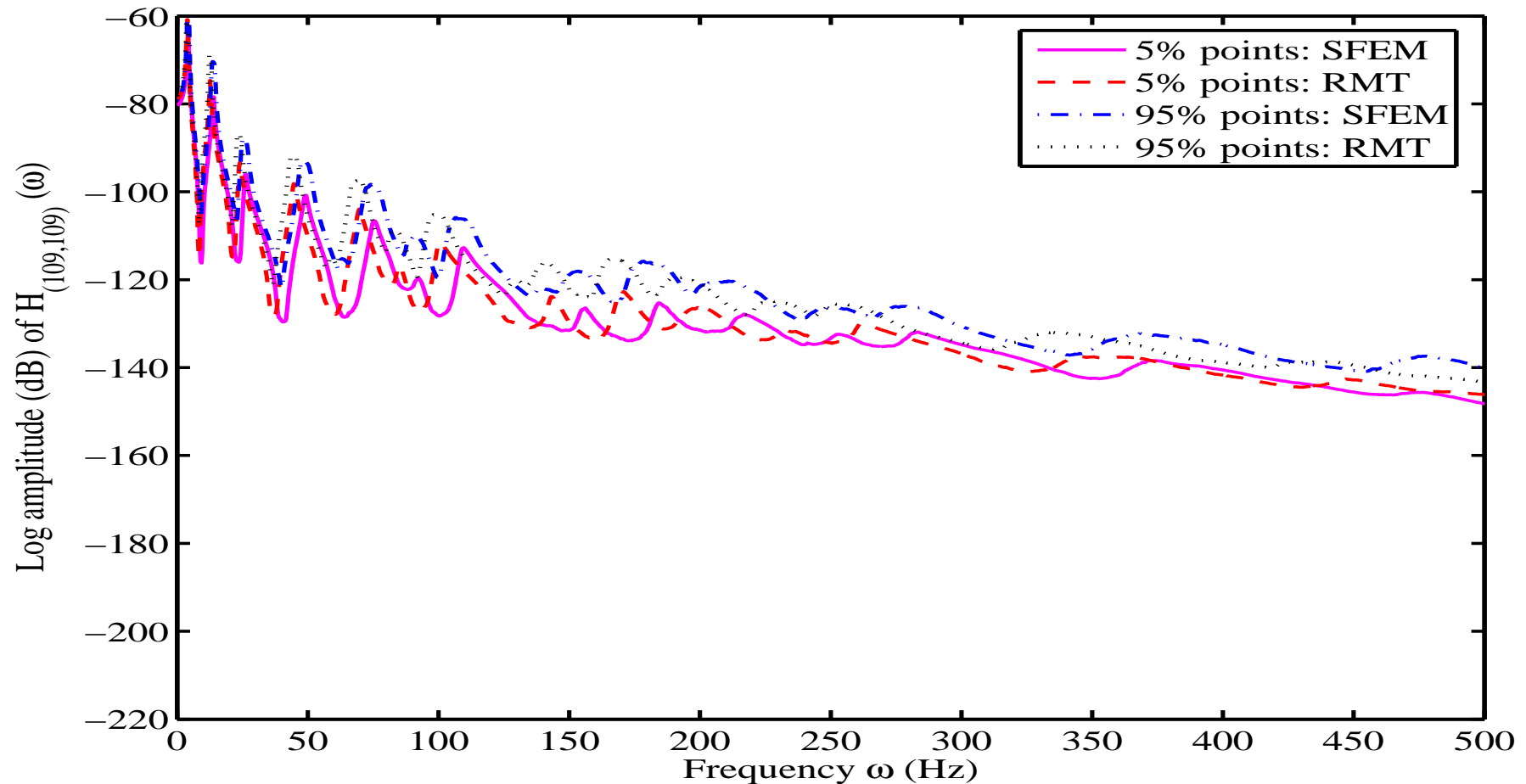
Comparison of the 5% and 95% probability points of the amplitude of the cross-FRF.

# Comparison of driving-point-FRF



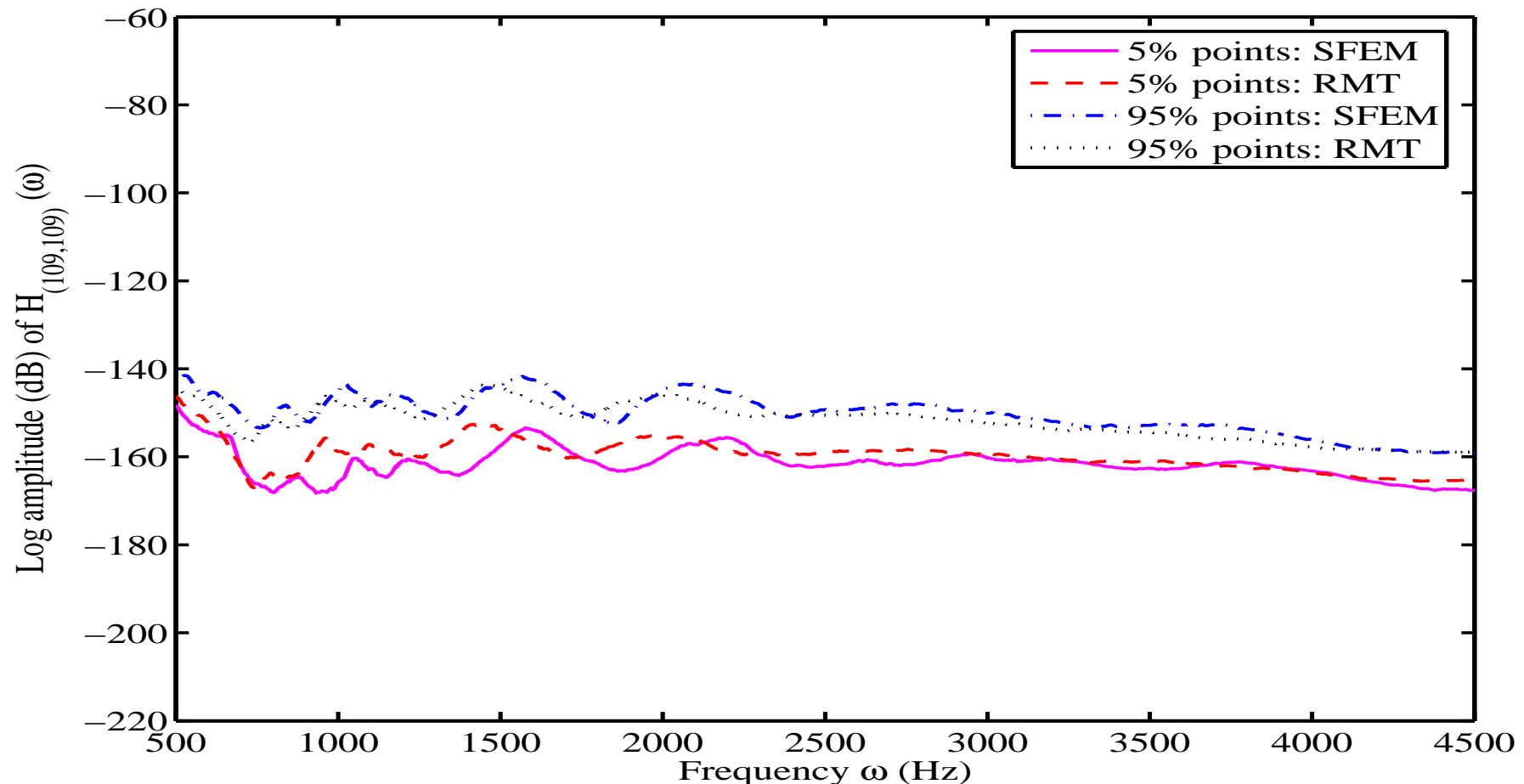
Comparison of the 5% and 95% probability points of the amplitude of the driving-point-FRF.

# Comparison of driving-point-FRF: Low Freq



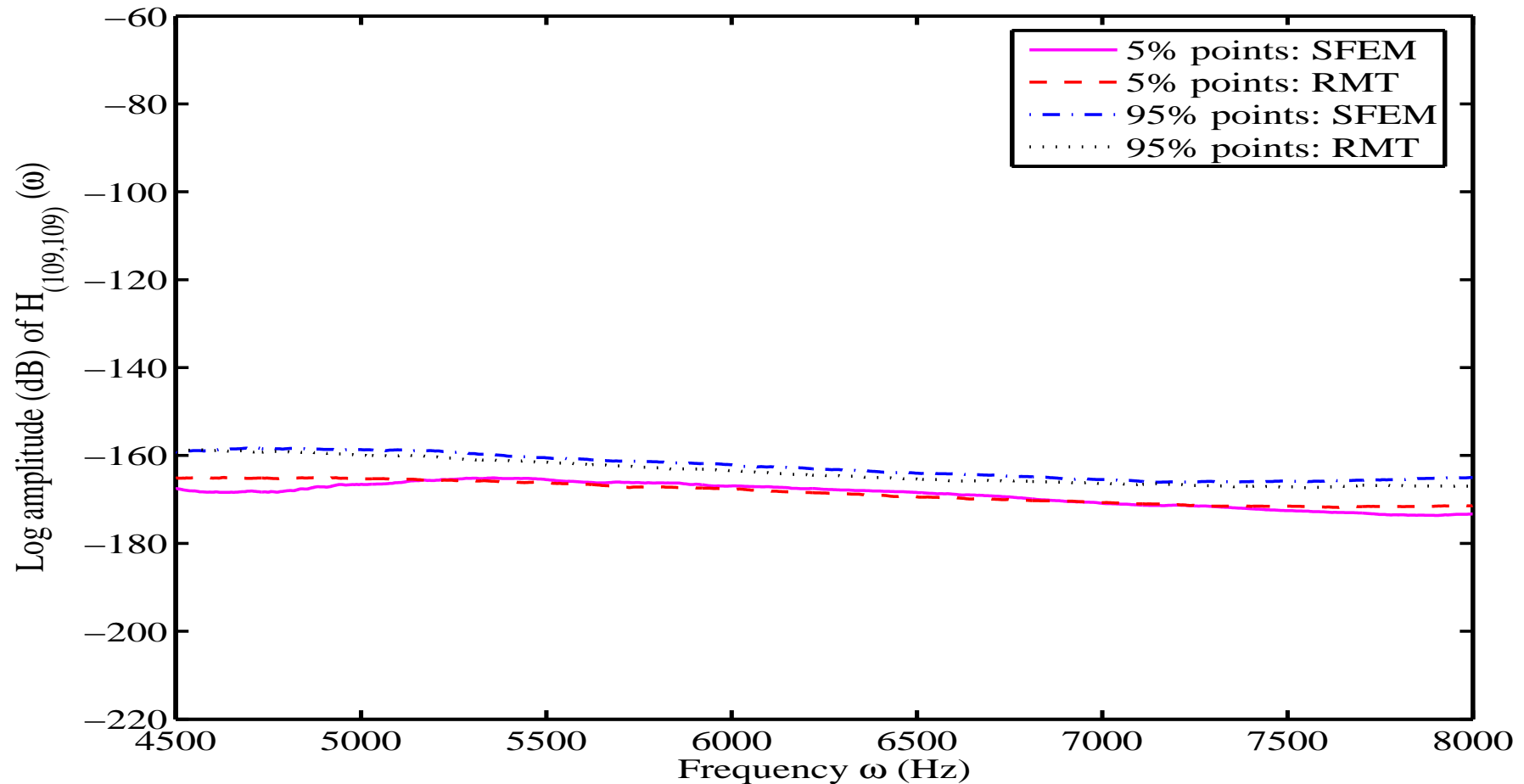
Comparison of the 5% and 95% probability points of the amplitude of the driving-point-FRF.

# Comparison of driving-point-FRF: Mid Freq



Comparison of the 5% and 95% probability points of the amplitude of the driving-point-FRF.

# Comparison of driving-point-FRF: High Freq



Comparison of the 5% and 95% probability points of the amplitude of the driving-point-FRF.

# Summary & conclusions

- **Wishart matrices** may be used as the model for the system matrices in structural dynamics.
- The parameters of the distribution were obtained in closed-form by solving an optimisation problem.
- Only the mean matrix and normalized standard deviation is required to model the system.
- Numerical results show that SFEM and RMT results match well in the mid and high frequency region.

# Next steps

- Eigenvalue and eigenvector statistics
- Steady-state and transient dynamic response statistics
- Distribution of the dynamic stiffness matrix (complex Wishart matrix?) and its inverse (FRF matrix)
- Cumulative distribution function of the response (reliability problem)



# Open issues & discussions

- $\overline{G}$  is just one ‘observation’ - not an ensemble mean.
- Are we taking account of model uncertainties (‘unknown unknowns’)?
- How to incorporate a given covariance tensor of  $G$  (e.g., obtained using the Stochastic Finite element Method)?
- What is the consequence of the zeros in  $G$  are not being preserved?